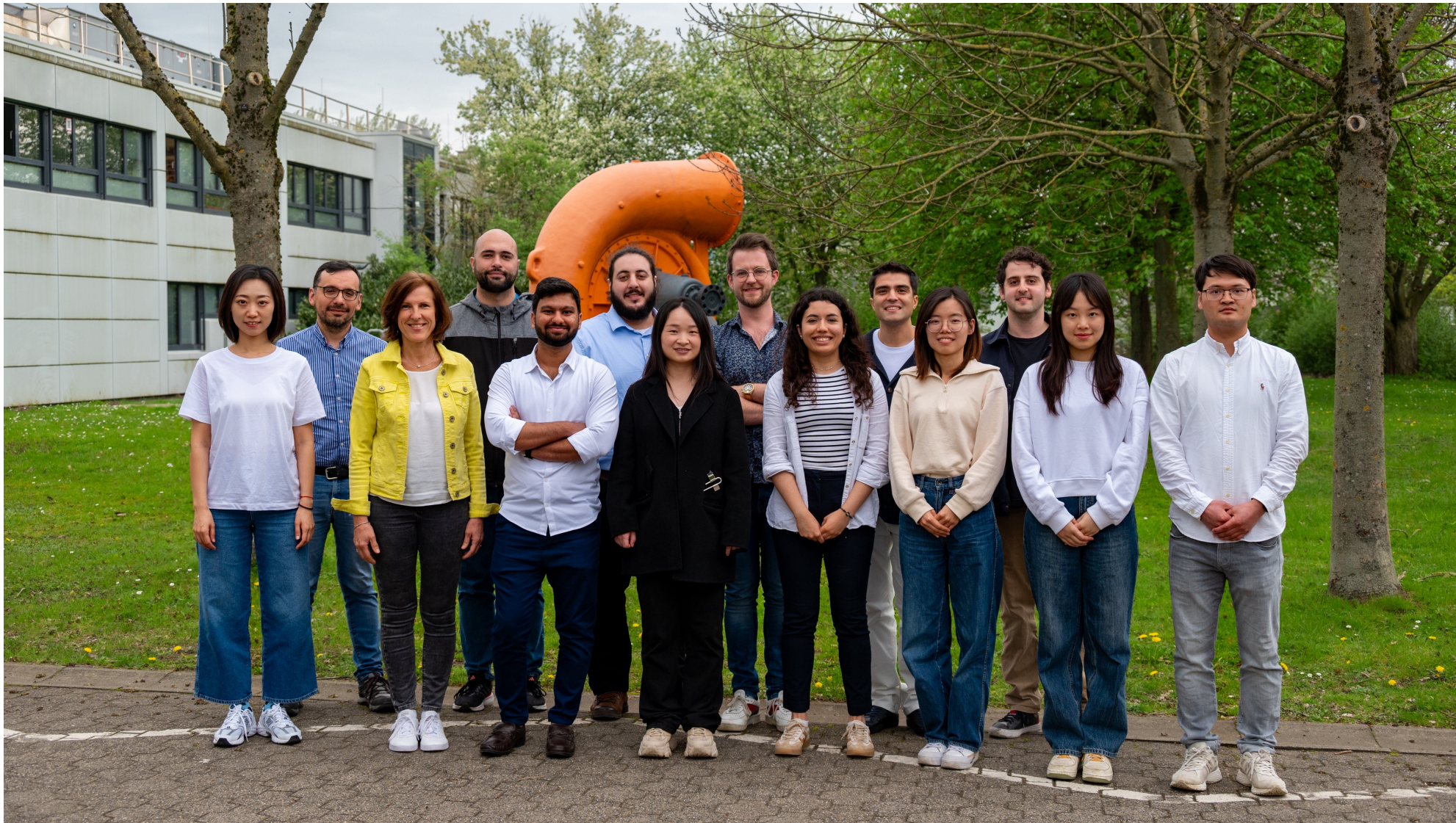


Quantification and propagation of uncertainties in expensive simulation models

Prof. Dr. Matthias Faes
Professor in Reliability Engineering
TU Dortmund University

A big thanks to the team @ CRE – TU Dortmund

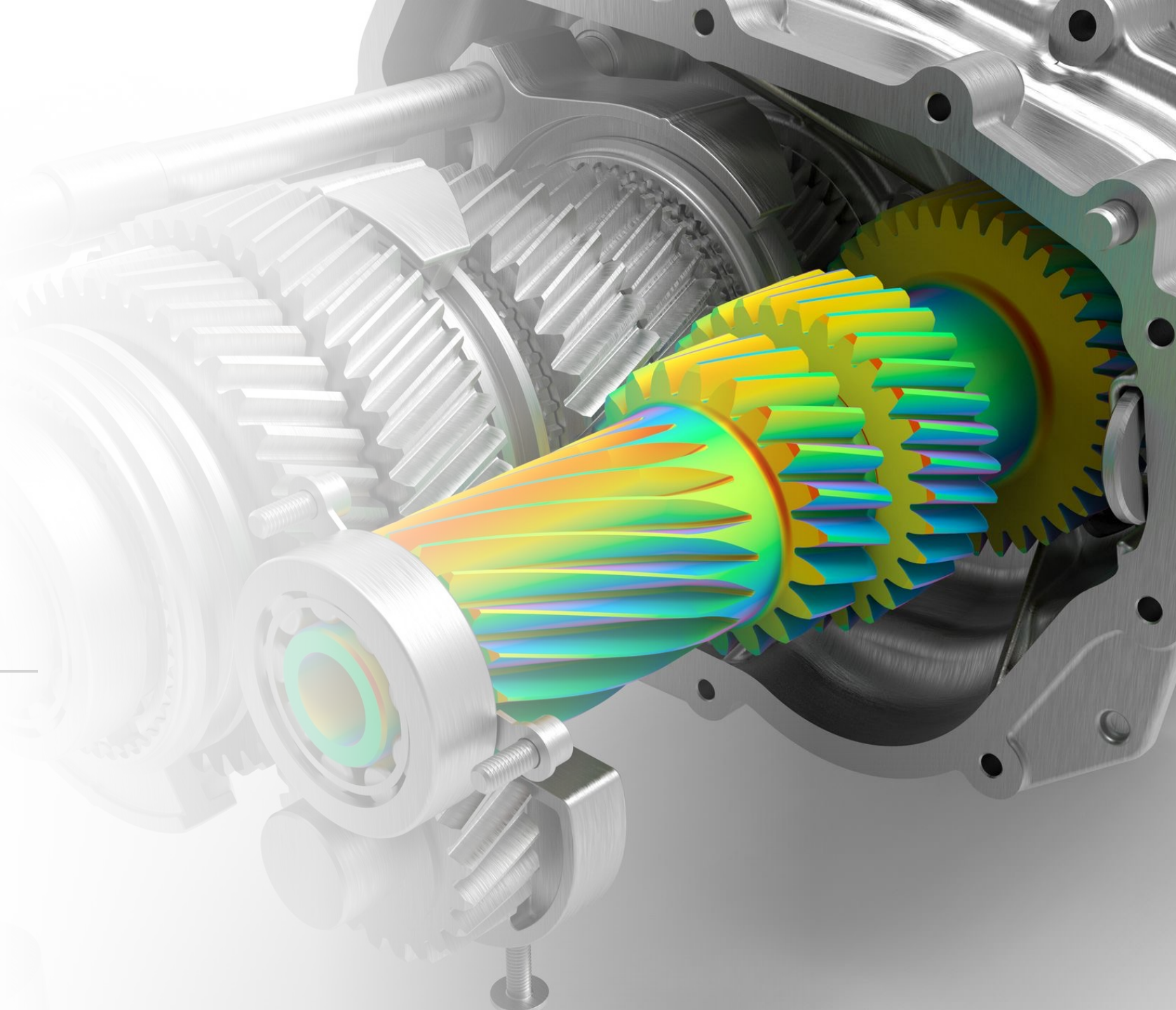


Not in the picture:





Numerical
simulation tools
allow for designing
complex
components



Computational models in engineering

- Complex engineering systems are designed and assessed using computational models
- A computational model consists of:
 - A mathematical description of the physical phenomena (i.e., the governing equations)
 - Discretisation techniques that transform continuous equations into linear algebraic formulations
 - Algorithms to solve the discretized equations

$$\operatorname{div} \boldsymbol{\sigma} + \mathbf{f} = 0$$

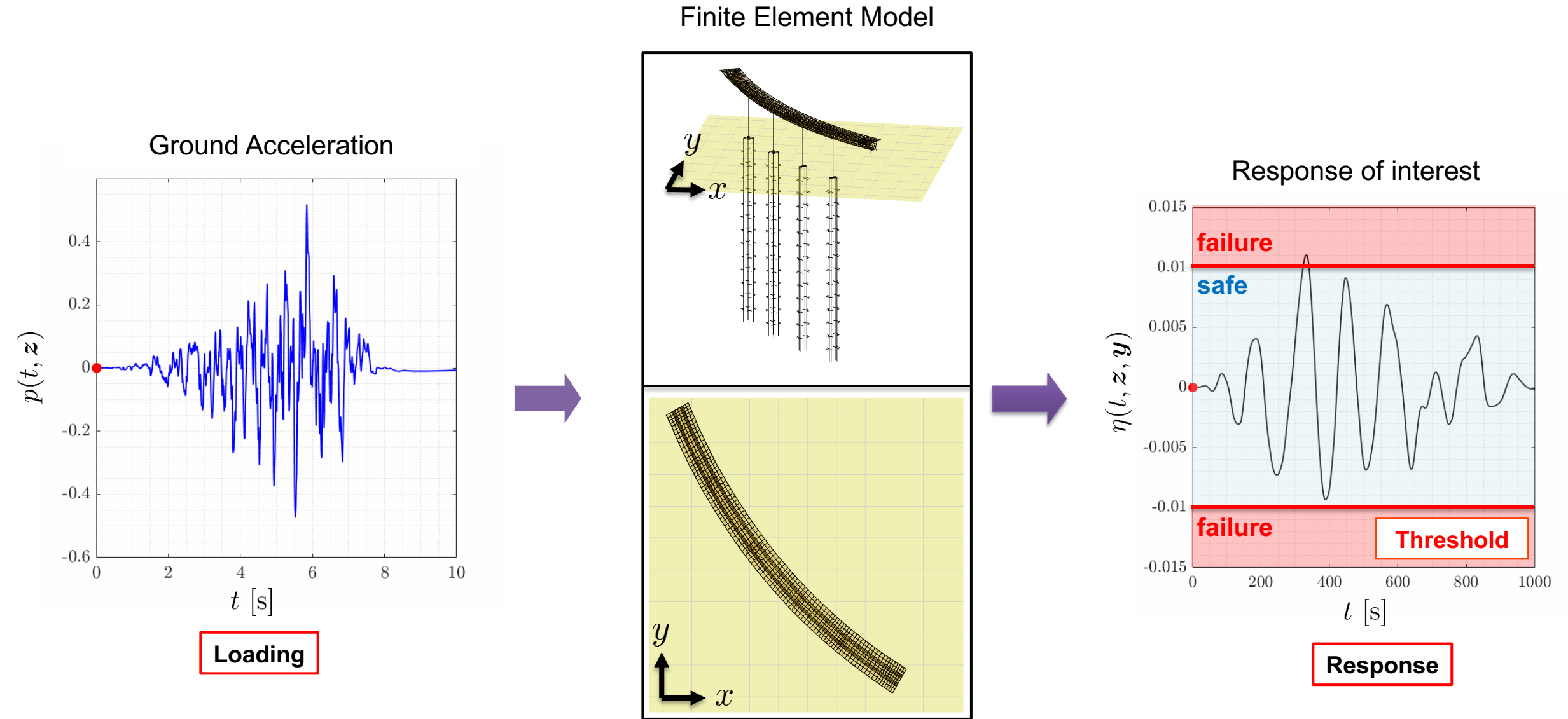
$$\boldsymbol{\sigma} = \mathbf{D} \cdot \boldsymbol{\epsilon}$$

$$\boldsymbol{\epsilon} = \frac{1}{2} (\Delta \mathbf{u} + {}^T \Delta \mathbf{u})$$



$$\begin{bmatrix} \mathbf{L} & \mathbf{A} & \mathbf{P} & \mathbf{A} & \mathbf{C} & \mathbf{K} \\ \mathbf{L} & -\mathbf{A} & \mathbf{P} & -\mathbf{A} & \mathbf{C} & -\mathbf{K} \\ \mathbf{L} & \mathbf{A} & \mathbf{P} & \mathbf{A} & -\mathbf{C} & -\mathbf{K} \\ \mathbf{L} & -\mathbf{A} & \mathbf{P} & -\mathbf{A} & -\mathbf{C} & \mathbf{K} \\ \mathbf{L} & \mathbf{A} & -\mathbf{P} & -\mathbf{A} & \mathbf{C} & \mathbf{K} \\ \mathbf{L} & -\mathbf{A} & -\mathbf{P} & \mathbf{A} & \mathbf{C} & -\mathbf{K} \end{bmatrix}$$

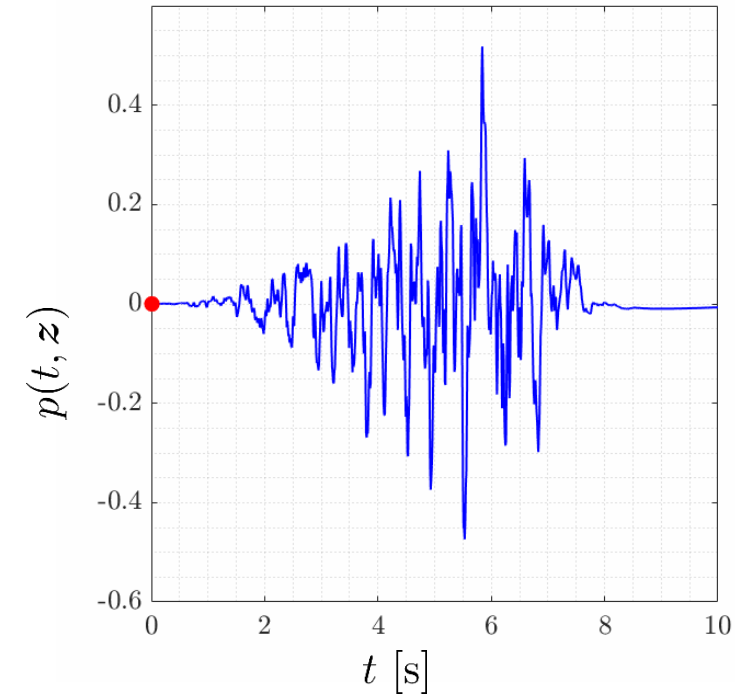
Computational models : another viewpoint



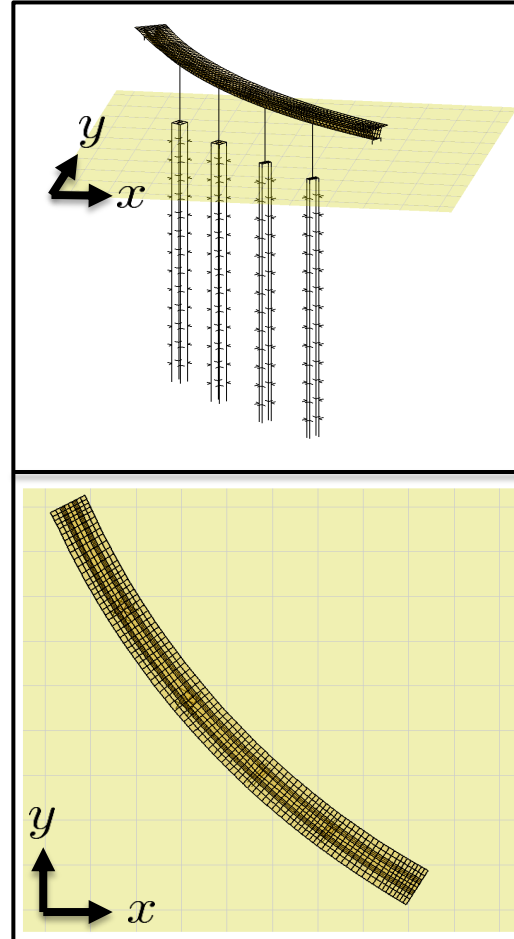
Computational models : another viewpoint

Finite Element Model

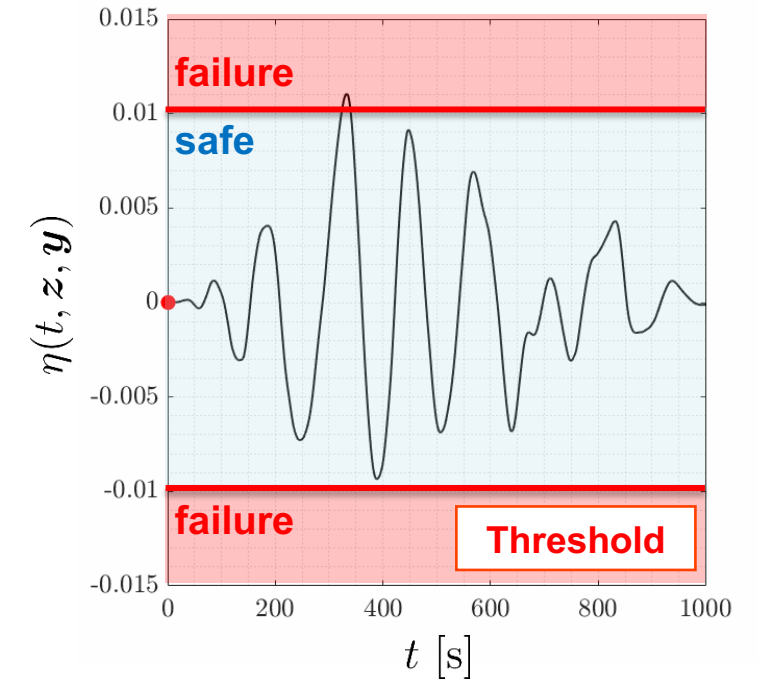
Ground Acceleration



Loading



Response of interest

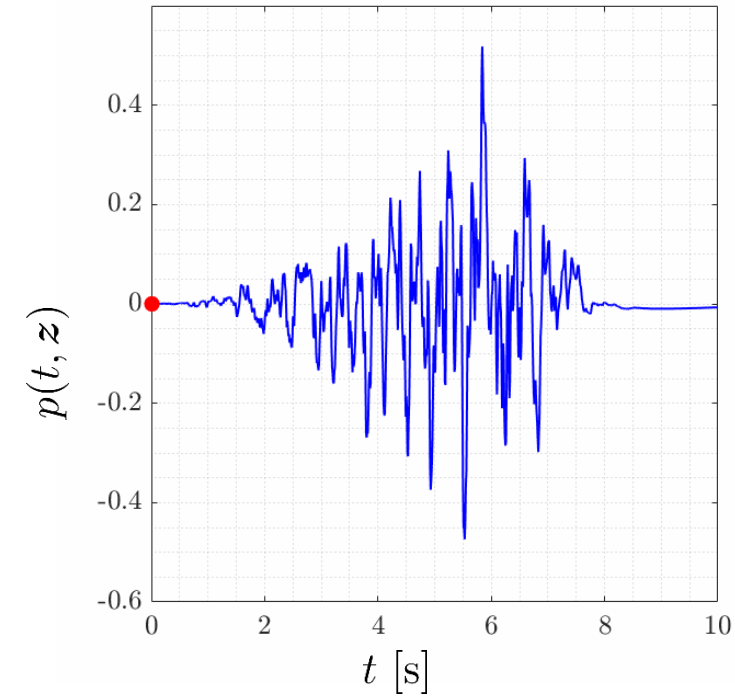


Response

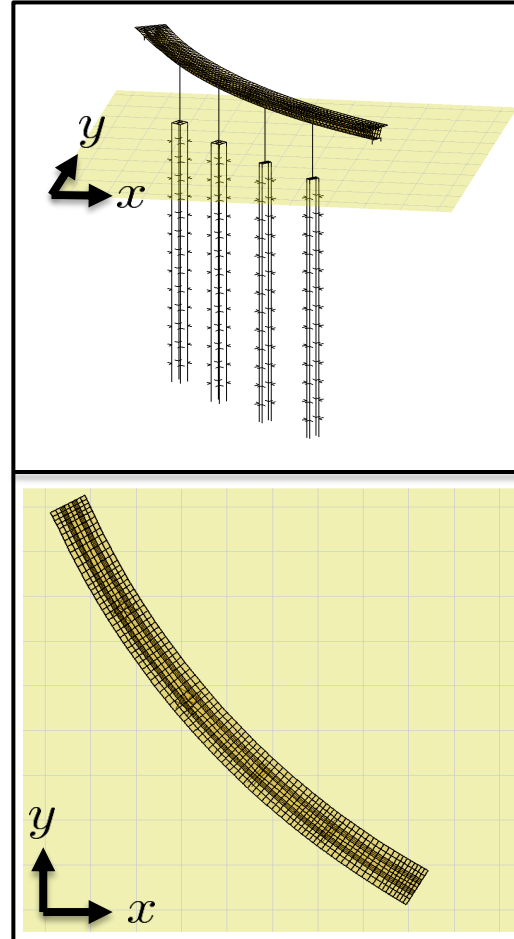
Computational models : another viewpoint

Finite Element Model

Ground Acceleration



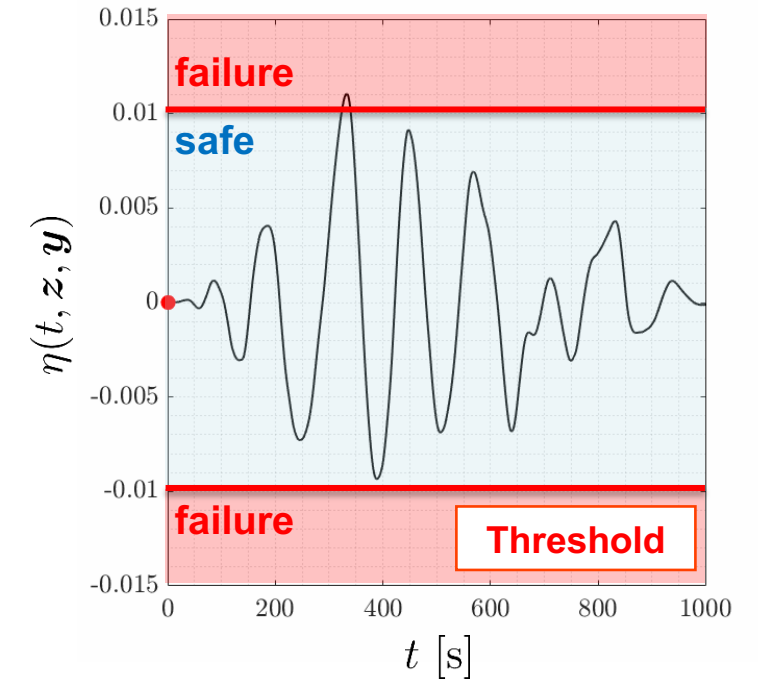
Stochastic process



Uncertain model properties

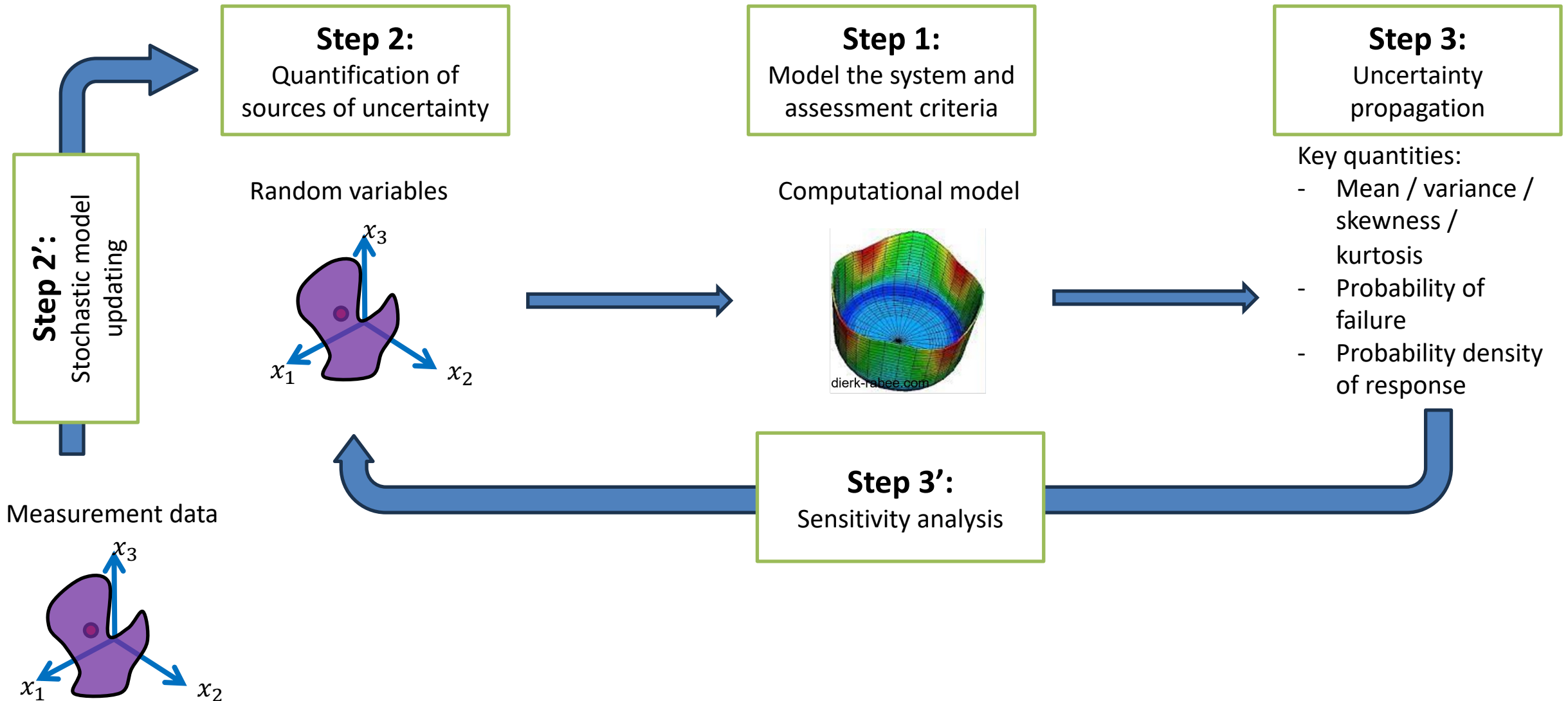


Response of interest

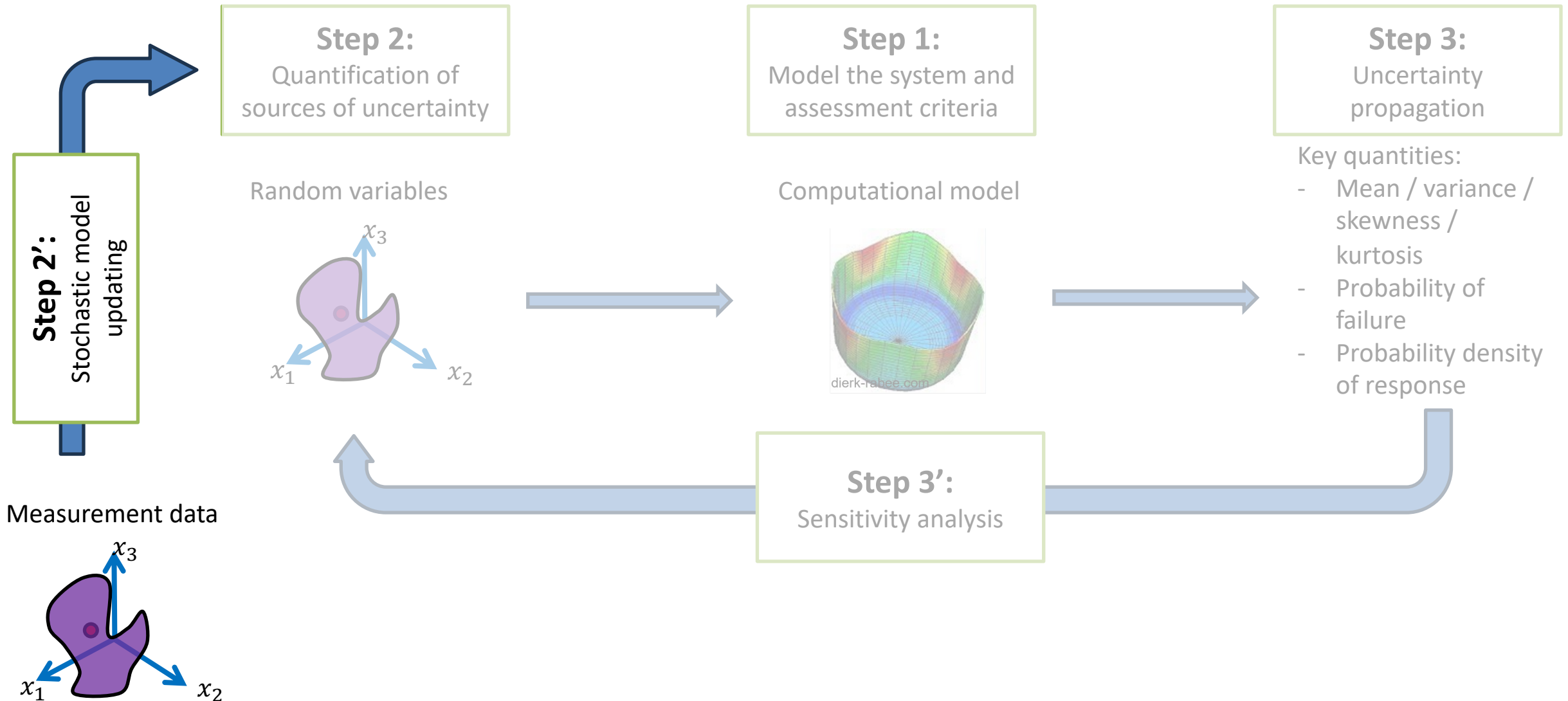


Stochastic response

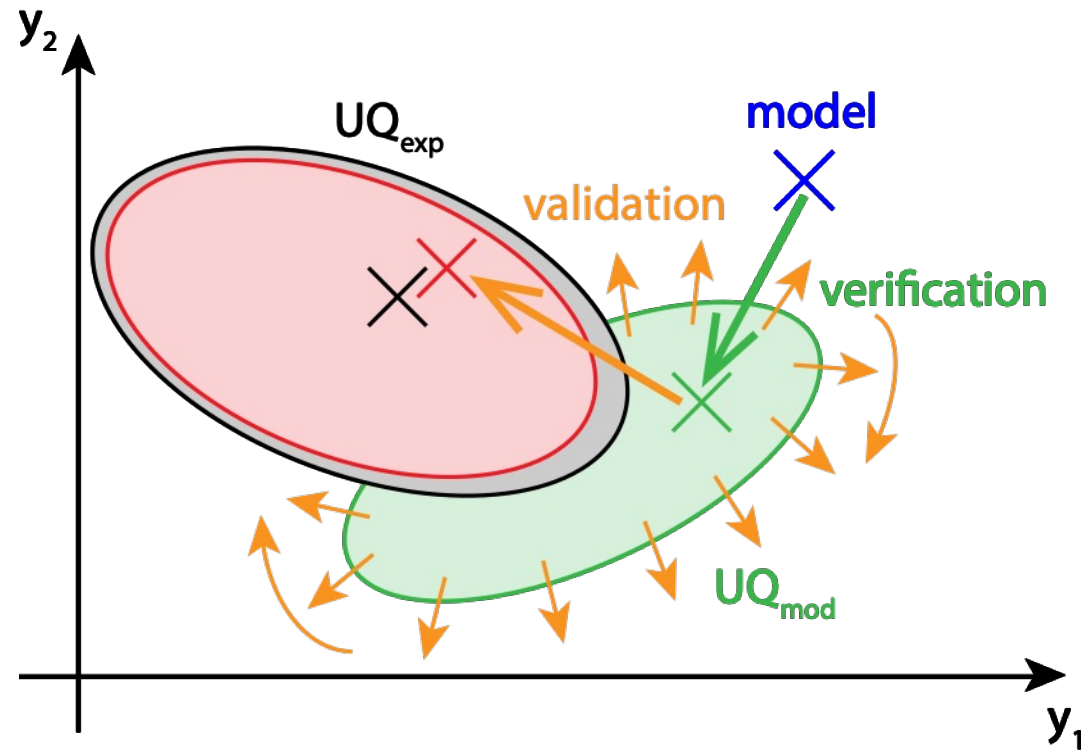
General uncertainty quantification overview



General uncertainty quantification overview



Step 2': Stochastic model updating



Step 1: modelling

Step 2: uncertainty
modelling

Step 2': stochastic
model updating

Experimental quantification of probabilistic variability

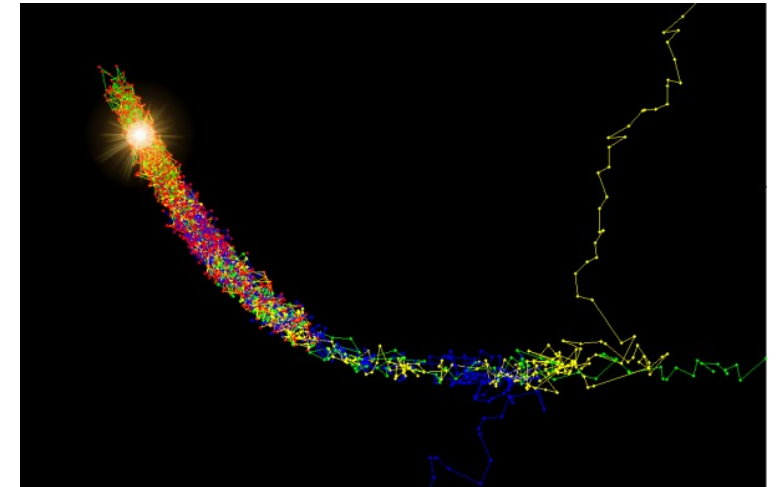
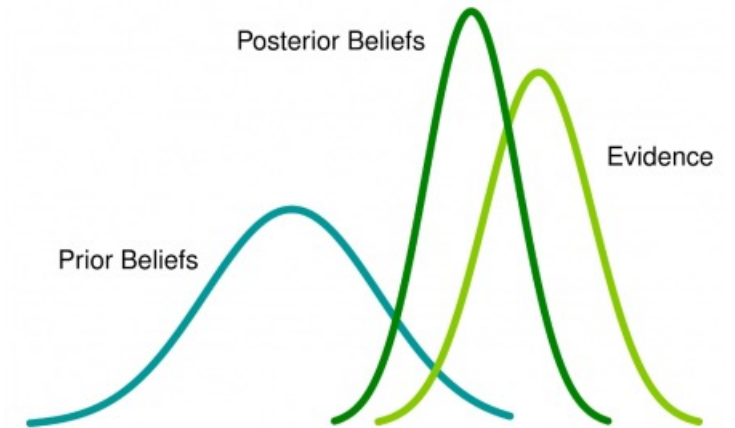
- Bayesian updating

$$f(\theta|D, M) = \frac{f(D|M, \theta) \cdot f(\theta|M)}{f(D|M)}$$

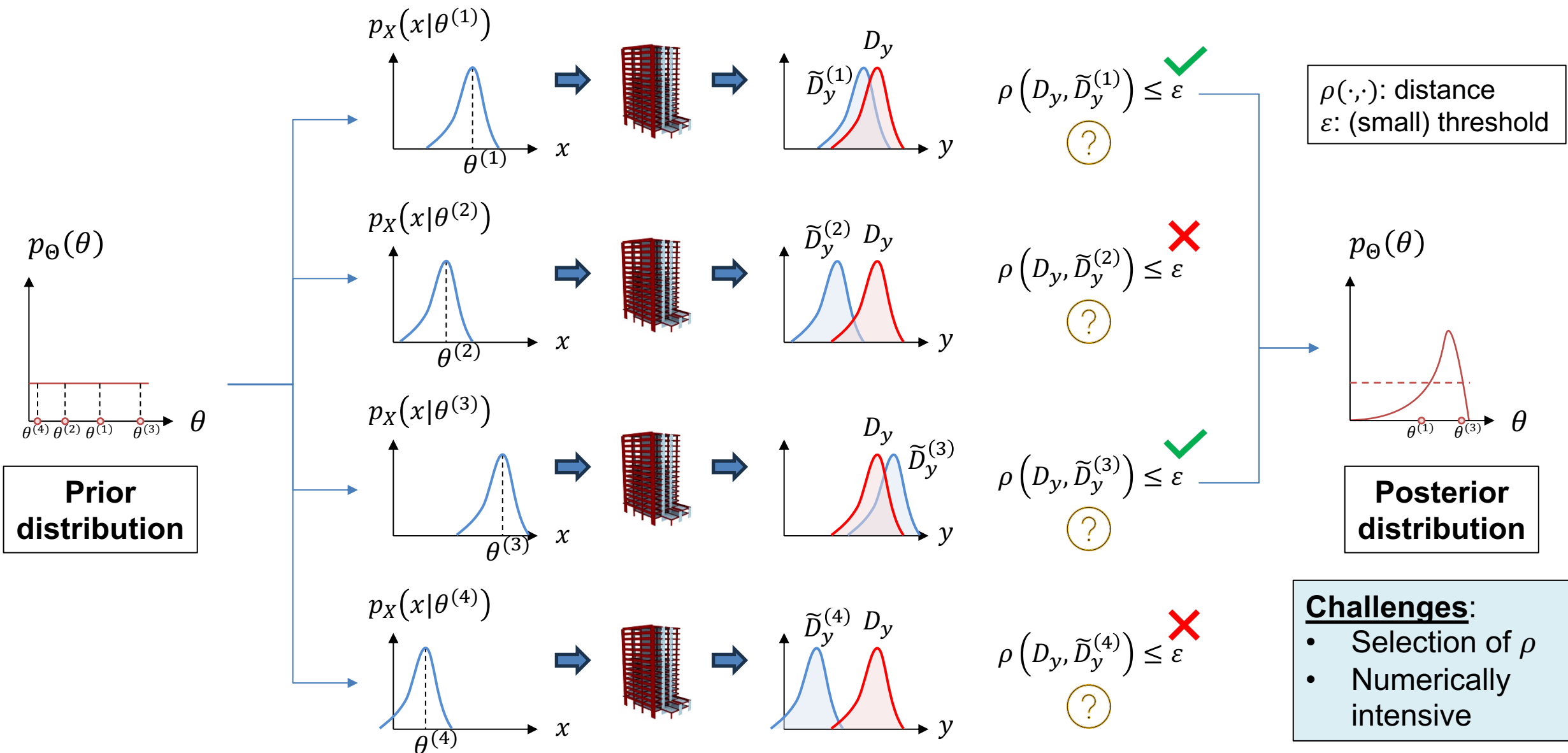
- $f(D|M, \theta)$ often based on a zero-mean Gaussian white noise with covariance Σ

$$f(D|M, \theta) \propto \prod_{i=1}^N \exp\left(-\frac{1}{2} \epsilon_i^T(\theta) \Sigma^{-1} \epsilon_i(\theta)\right)$$

- Model evidence $f(D|M)$ is a tool for model selection
- However:
 - Need for expensive Markov Chain Monte Carlo based simulators (MCMC, TMCMC, HMCMC)
 - Gaussian assumption of error usually not realistic

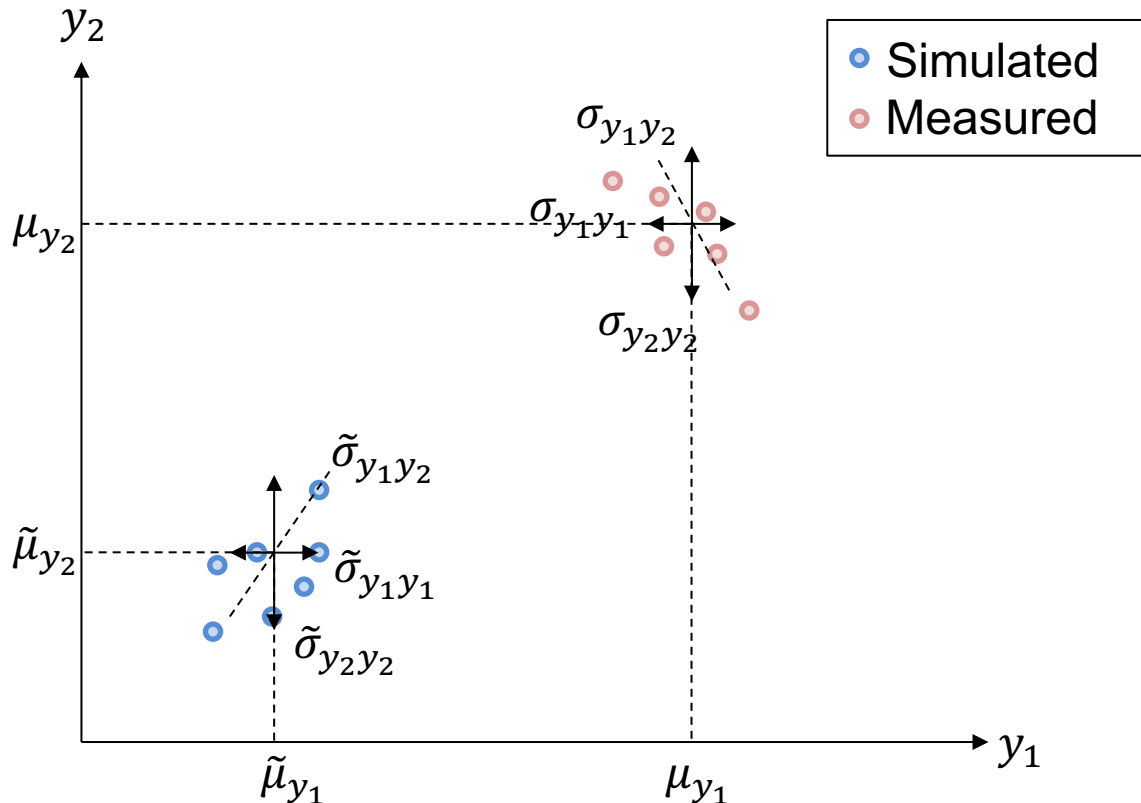


Approximate Bayesian Computation (ABC)



Distance ρ : Selection

- Different distance metrics available, e.g. Euclidian distance, Mahalanobis distance, Bhattacharyya distance, etc.
- This contribution: **summary statistics**



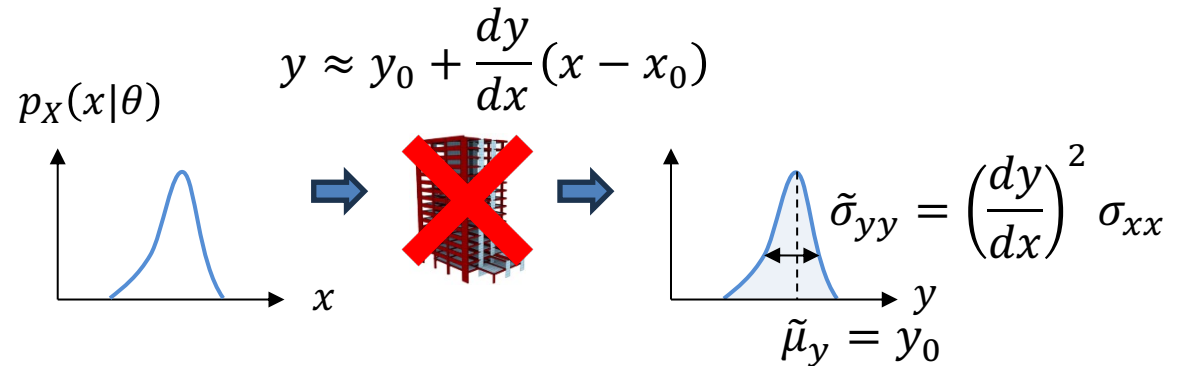
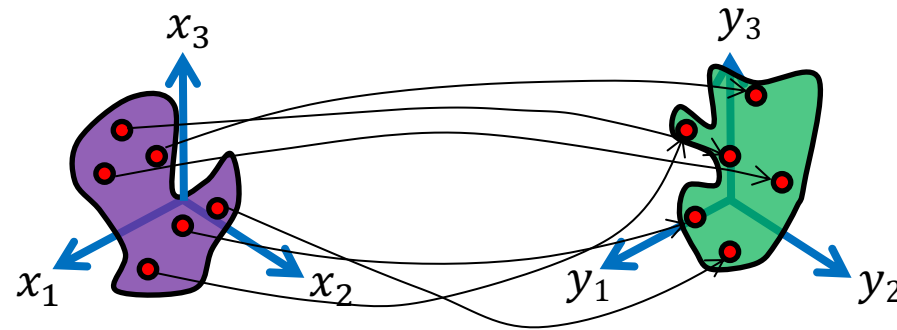
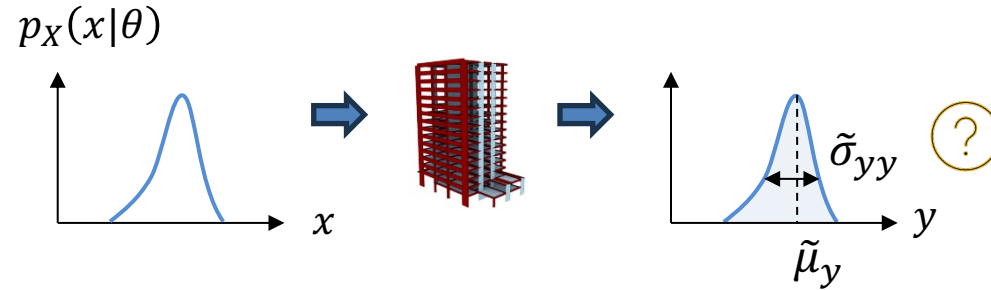
$\rho(D_y, \tilde{D}_y)$: maximum relative difference between **second order statistics** of simulated and measured data

Distance ρ : Calculation

- Distance ρ demands knowledge on **mean** and **covariance** of simulated data

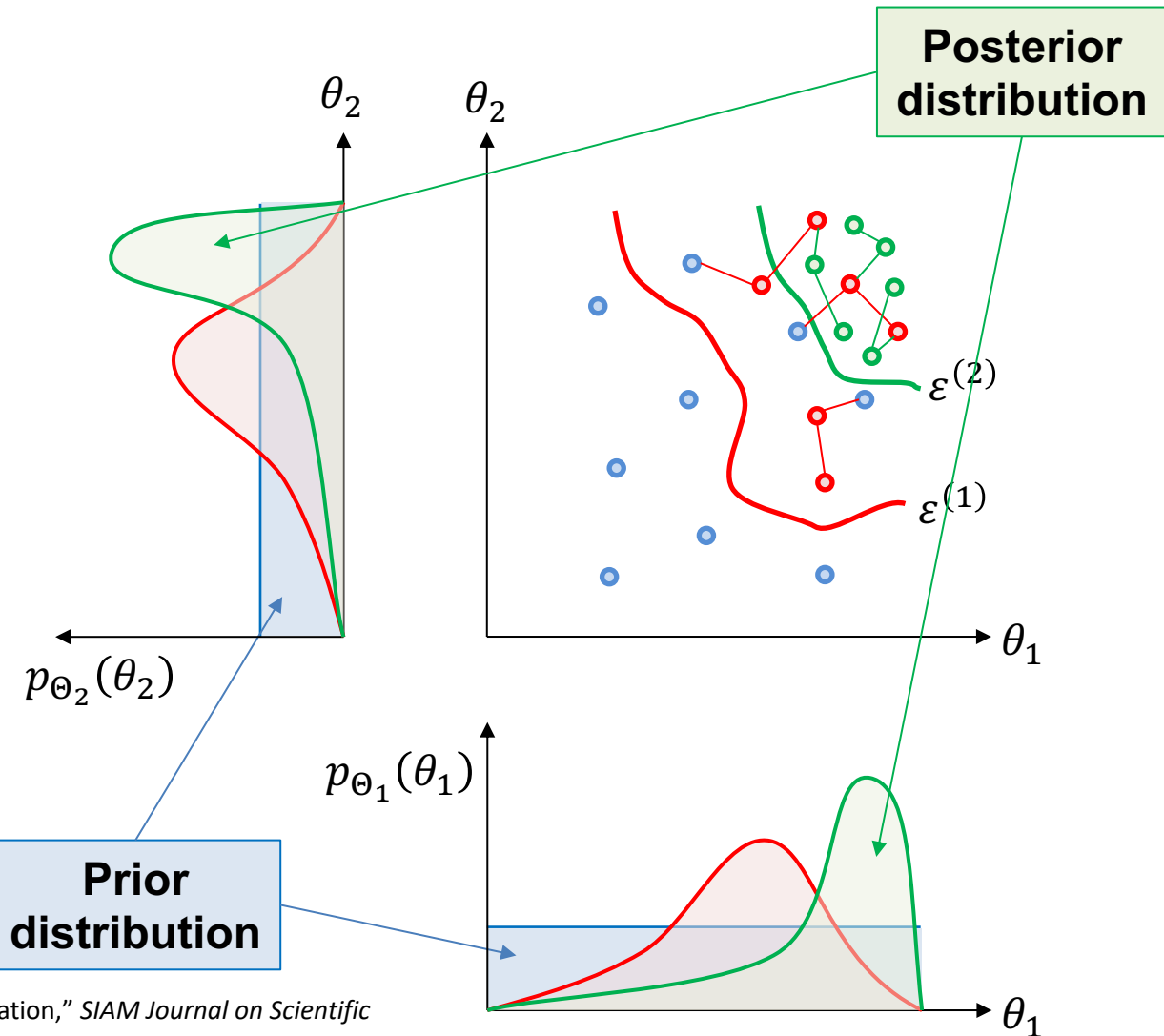
- Monte Carlo simulation+divergence: accurate but numerically demanding, noisy estimators

- **Perturbation**: accuracy depends on nonlinearity, highly efficient, precise estimators



Practical Implementation: Subset Simulation

- Subset simulation*
 - Small batches of simulated data at each stage
 - Threshold levels $\varepsilon^{(1)} \geq \varepsilon^{(2)} \geq \dots$ selected adaptively
 - **Gradual approach** from prior to sought posterior distribution
 - Samples of θ conditioned on $\rho \geq \varepsilon^{(i)}$ are generated with **preconditioned Crank – Nicolson** algorithm**

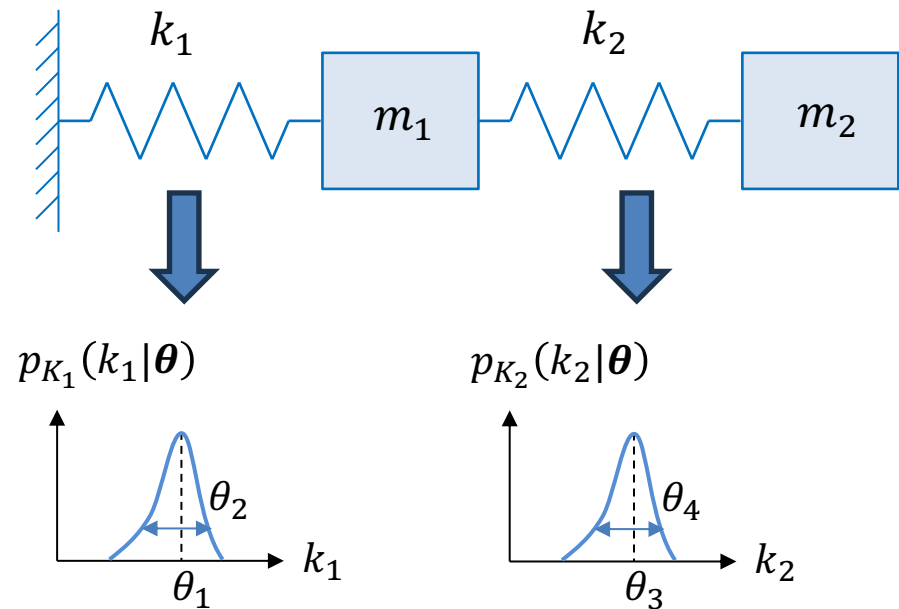


*M. Chiachio, J. L. Beck, J. Chiachio, and G. Rus, "Approximate Bayesian computation by subset simulation," *SIAM Journal on Scientific Computing*, vol. 36, Art. no. 3, 2014.

**A. Beskos, G. Roberts, A. Stuart, and J. Voss, "MCMC methods for diffusion bridges," *Stochastics and Dynamics*, vol. 8, Art. no. 03, 2008.

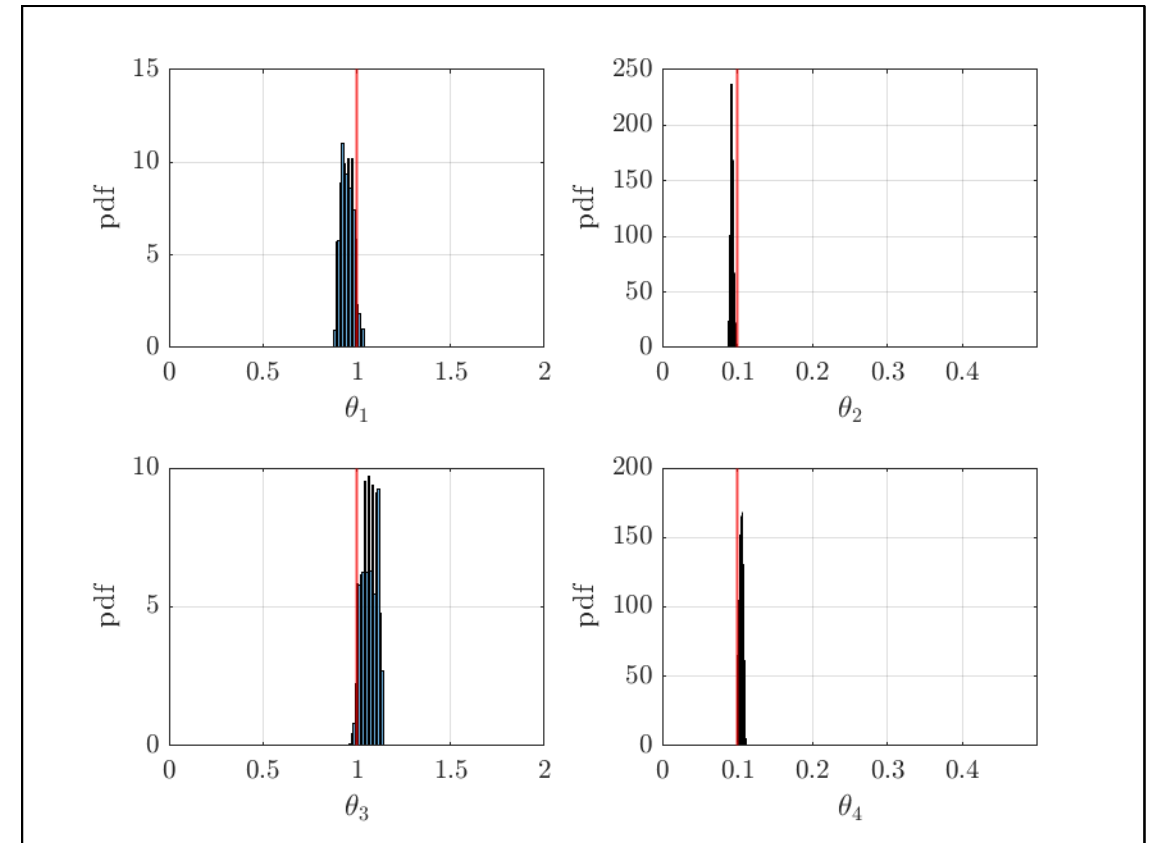
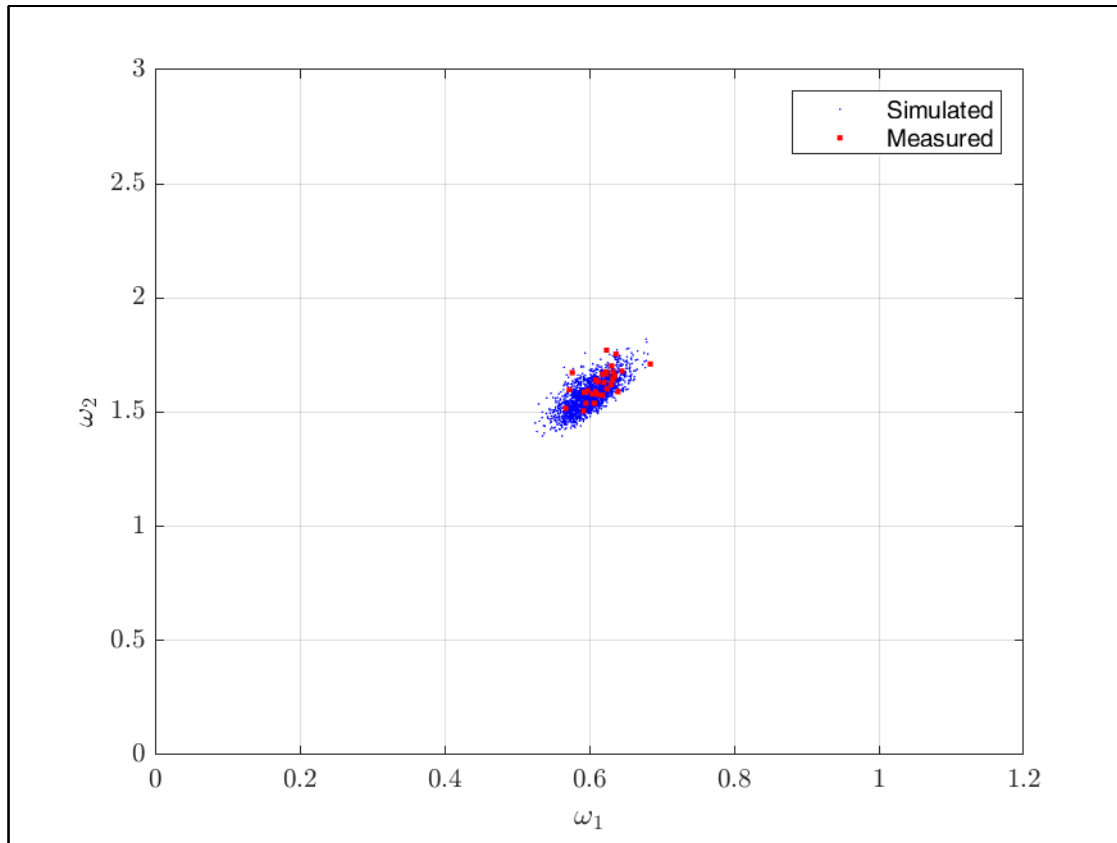
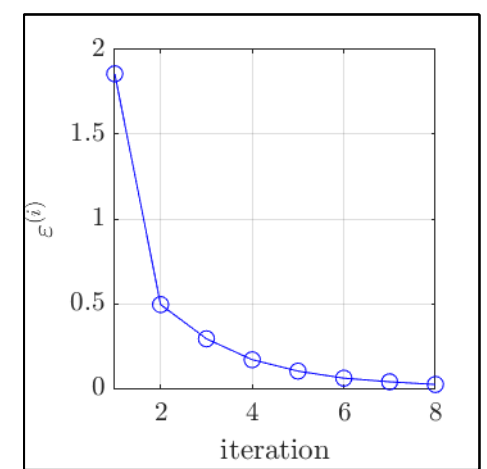
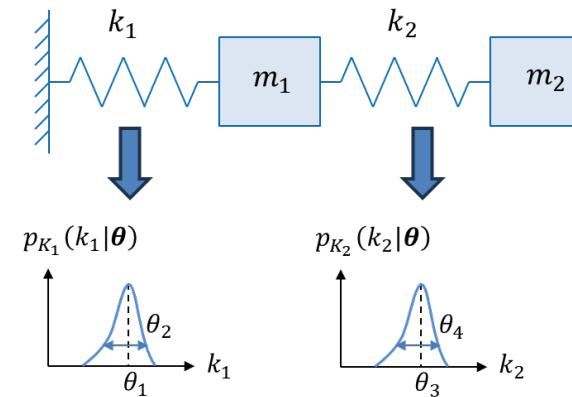
Example

- Two-degree-of-freedom oscillator
 - Uncertain stiffnesses k_1 and k_2 (lognormal distribution)
 - Epistemic uncertainty regarding mean value (θ_1, θ_3) and standard deviation (θ_2, θ_4) of each stiffness
 - 30 measurements of natural frequencies (synthetically generated)

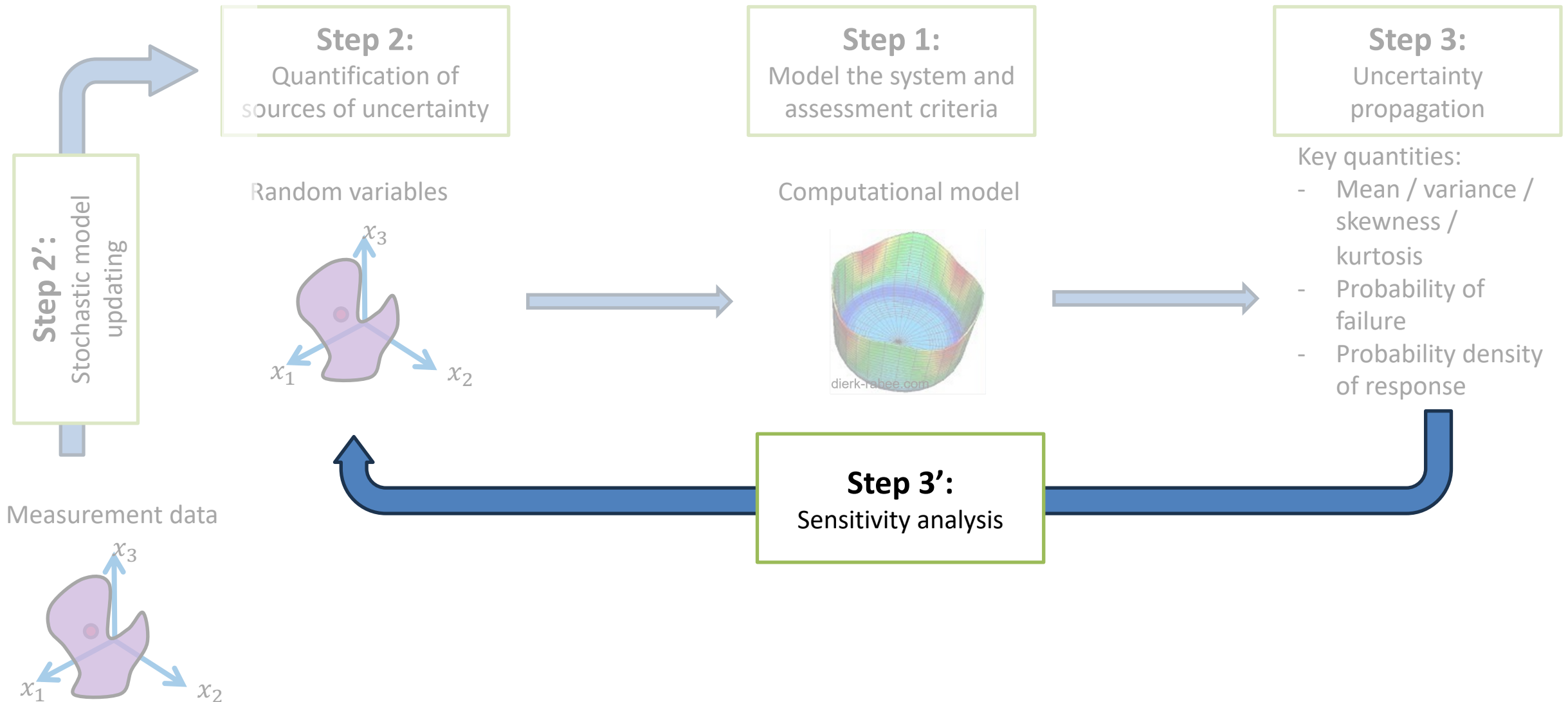


Example

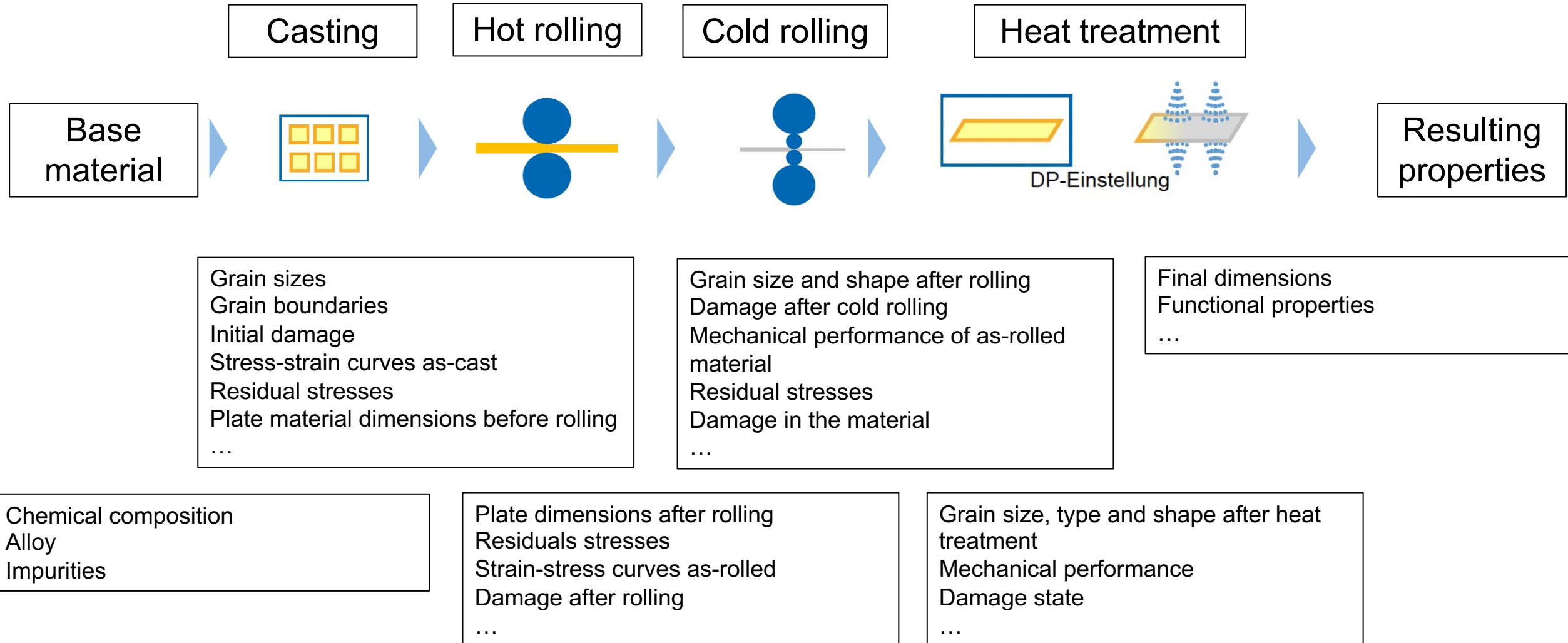
- Two-degree-of-freedom oscillator



General uncertainty quantification overview



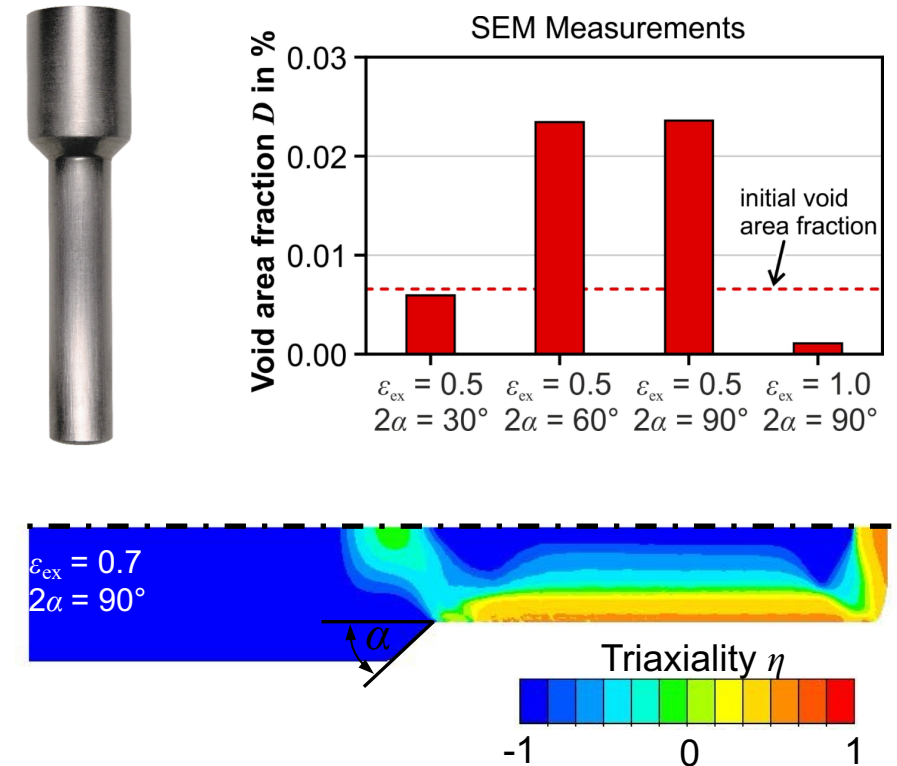
Step 3': sensitivity analysis



Application of probabilistic methods in metal forming

- Damage is introduced during forward rod extrusion process
- Goal: predict damage numerically to optimize process a priori and *in silico*
- Challenge: many sources of uncertainty
 - Material parameters
 - Elastic
 - Damage model
 - Manufacturing parameters
 - Friction in the die
 - Flow characteristics

- Need for sensitivity analysis!



Böddecker, M., Faes, M., Menzel, A., Valdebenito, M. (2023). Effect of uncertainty of material parameters on stress triaxiality and Lode angle in finite elasto-plasticity - a variance-based global sensitivity analysis. Advances in Industrial and Manufacturing Engineering. Volume 7, November 2023, 100128

Application of probabilistic methods in metal forming

- First order sensitivity index (S_i)
 - Fraction of the variance of y that can be attributed to θ_i alone

$$\Rightarrow S_i = \frac{\mathbb{V}_{\Theta_i} [\mathbb{E}_{\Theta_{-i}} [y|\theta_i]]}{\mathbb{V}_{\Theta} [y]}$$

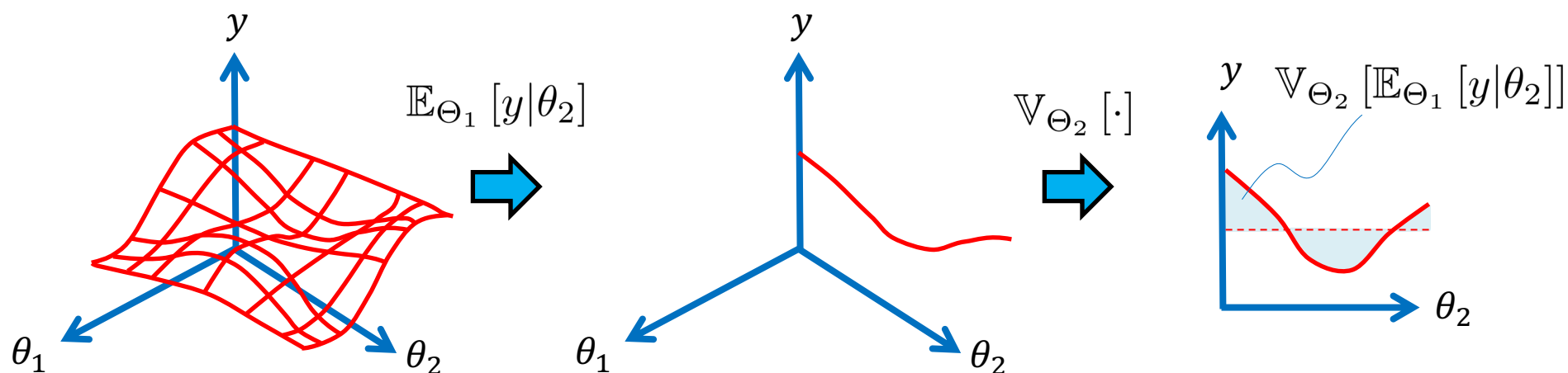
$\mathbb{E}_{\Theta}[\cdot]$: Expected value w.r.t. Θ

$\mathbb{V}_{\Theta}[\cdot]$: Variance w.r.t. Θ

$\Theta = \{\Theta_1, \dots, \Theta_{n_\theta}\}$

$\Theta_{-i} = \{\Theta_1, \dots, \Theta_{i-1}, \Theta_{i+1}, \Theta_{n_\theta}\}$

- Example: calculation of S_2 for model $y(\theta_1, \theta_2)$

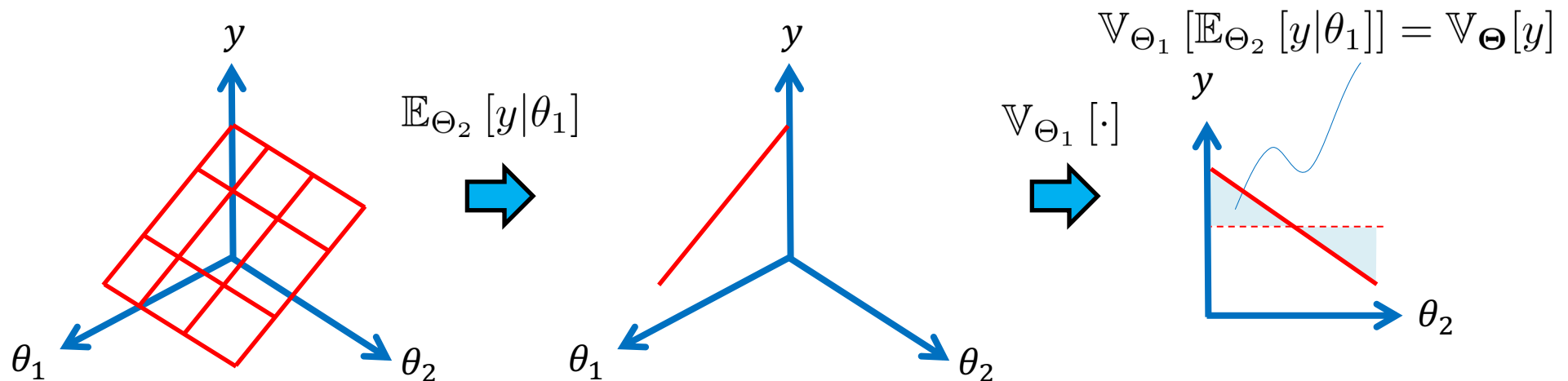


Application of probabilistic methods in metal forming

- Total sensitivity index (S_{T_i})
 - Fraction of the variance of y that can be attributed to θ_i and all its interactions with other variables

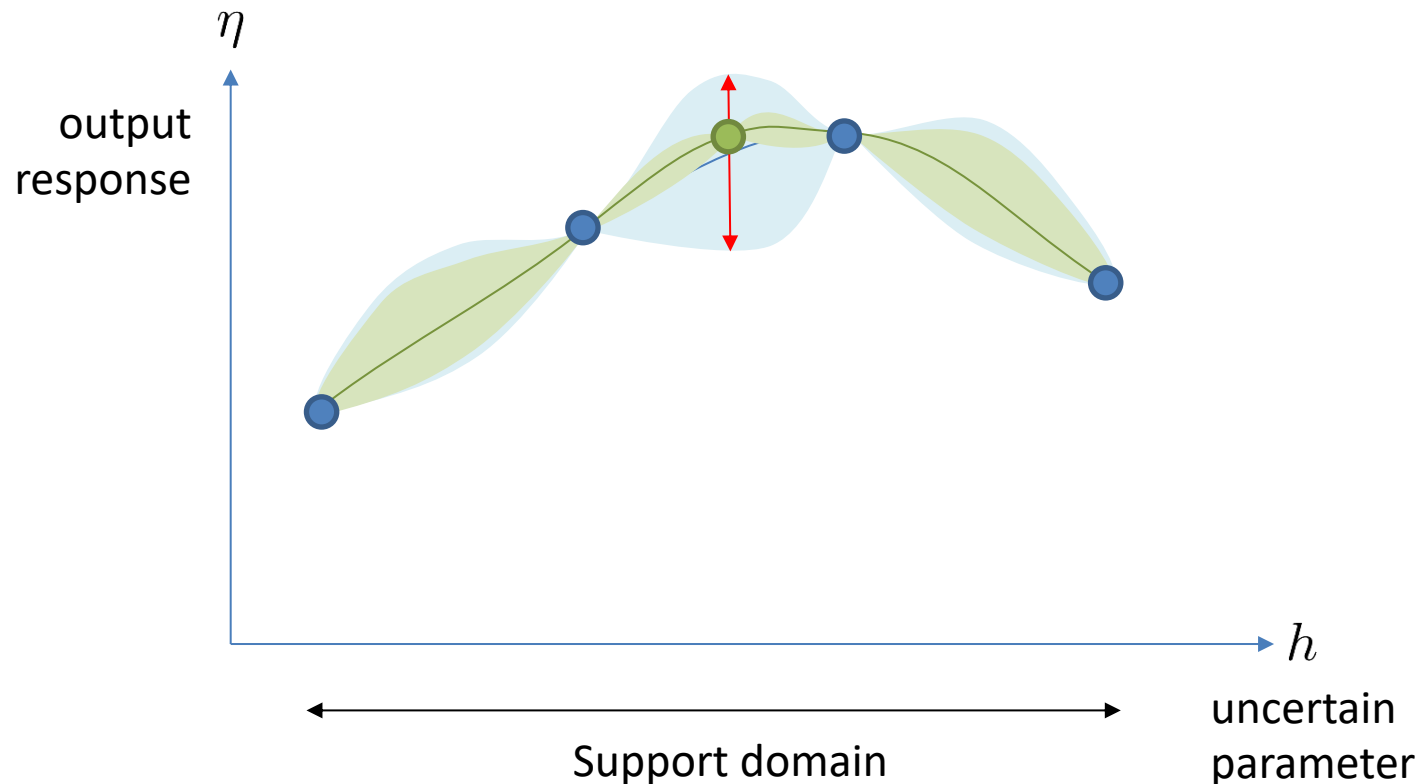
$$\Rightarrow S_{T_i} = 1 - \frac{\mathbb{V}_{\Theta_{-i}} [\mathbb{E}_{\Theta_i} [y|\boldsymbol{\theta}_{-i}]]}{\mathbb{V}_{\Theta} [y]}$$

- Example: calculation of S_{T_2} for model $y(\theta_1, \theta_2)$, $S_{T_2} = 0$



Application of probabilistic methods in metal forming

- Surrogate model is used to replace finite element simulations
- Bayesian active learning for Sobol indices



(1) Design of experiments /
full system analyses

(2) Interpolation & confidence
bounds

(3) Active learning / locate
critical point

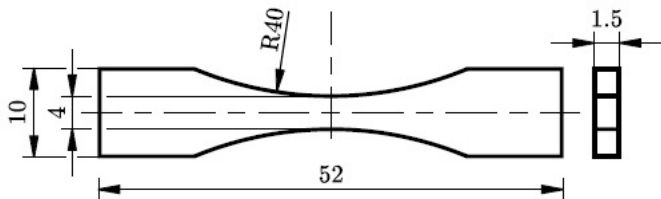
(4) Additional system analysis

(5) Improve surrogate

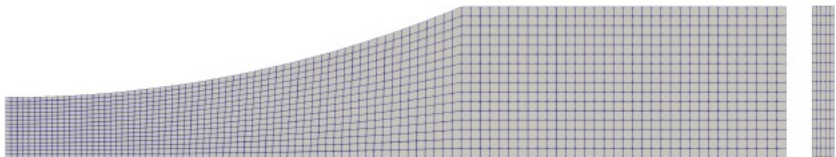
Application of probabilistic methods in metal forming

- Summary of results (1/2)

Model

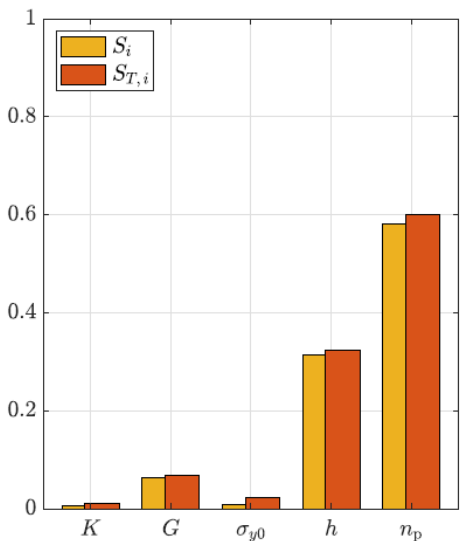


(a) Tensile test specimen geometry and dimensions.



(b) Spatial discretization of the tensile test specimen.

Results



(a) First-order and total order Sobol' sensitivity indices S_i and $S_{T,i}$ associated with maximum stress triaxiality η .

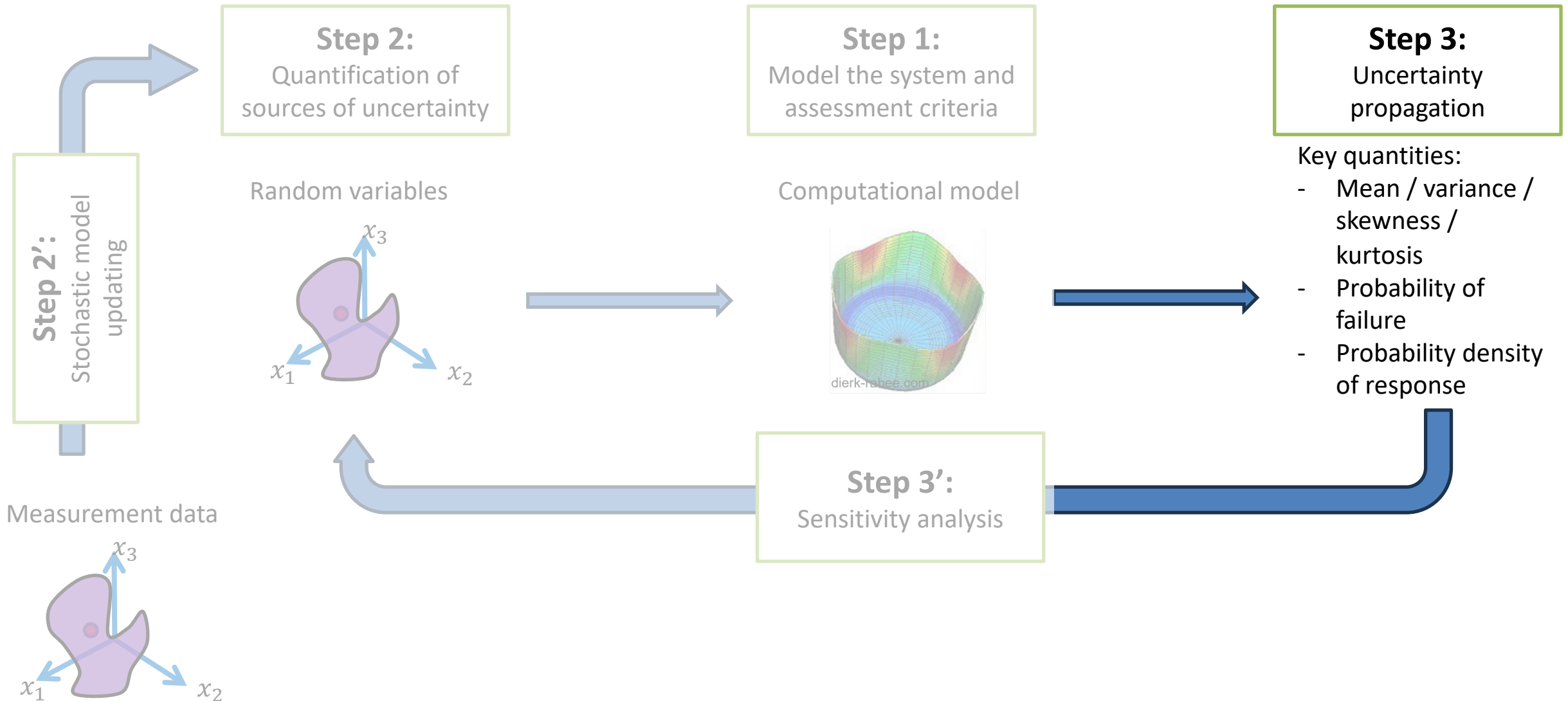
Table 3

First-order and total Sobol' sensitivity indices of stress triaxiality before active learning for different n_d and after convergence.

n_d	S_K [-]	S_G [-]	$S_{\sigma_{y0}}$ [-]	S_h [-]	S_{n_p} [-]
10	0.0000	0.1394	0.0000	0.3586	0.4857
30	0.0133	0.0812	0.0255	0.2778	0.5640
60	0.0185	0.0530	0.0075	0.3125	0.5682
60 + 145	0.0065	0.0622	0.0087	0.3134	0.5825
	$S_{T,K}$ [-]	$S_{T,G}$ [-]	$S_{T,\sigma_{y0}}$ [-]	$S_{T,h}$ [-]	S_{T,n_p} [-]
10	0.0000	0.1550	0.0000	0.3721	0.5027
30	0.0236	0.0915	0.0443	0.2938	0.6006
60	0.0322	0.0662	0.0134	0.3403	0.5980
60 + 145	0.0107	0.0690	0.0221	0.3234	0.6015

Böddecker, M., Faes, M., Menzel, A., Valdebenito, M. (2023). Effect of uncertainty of material parameters on stress triaxiality and Lode angle in finite elasto-plasticity - a variance-based global sensitivity analysis. Advances in Industrial and Manufacturing Engineering. Volume 7, November 2023, 100128

General uncertainty quantification overview



Step 3: uncertainty propagation

Gaussian Loading



$$p(t, z)$$

Structural Properties



$$\mathbf{y} = \begin{Bmatrix} y_1 \\ y_2 \\ y_3 \\ \dots \end{Bmatrix}$$

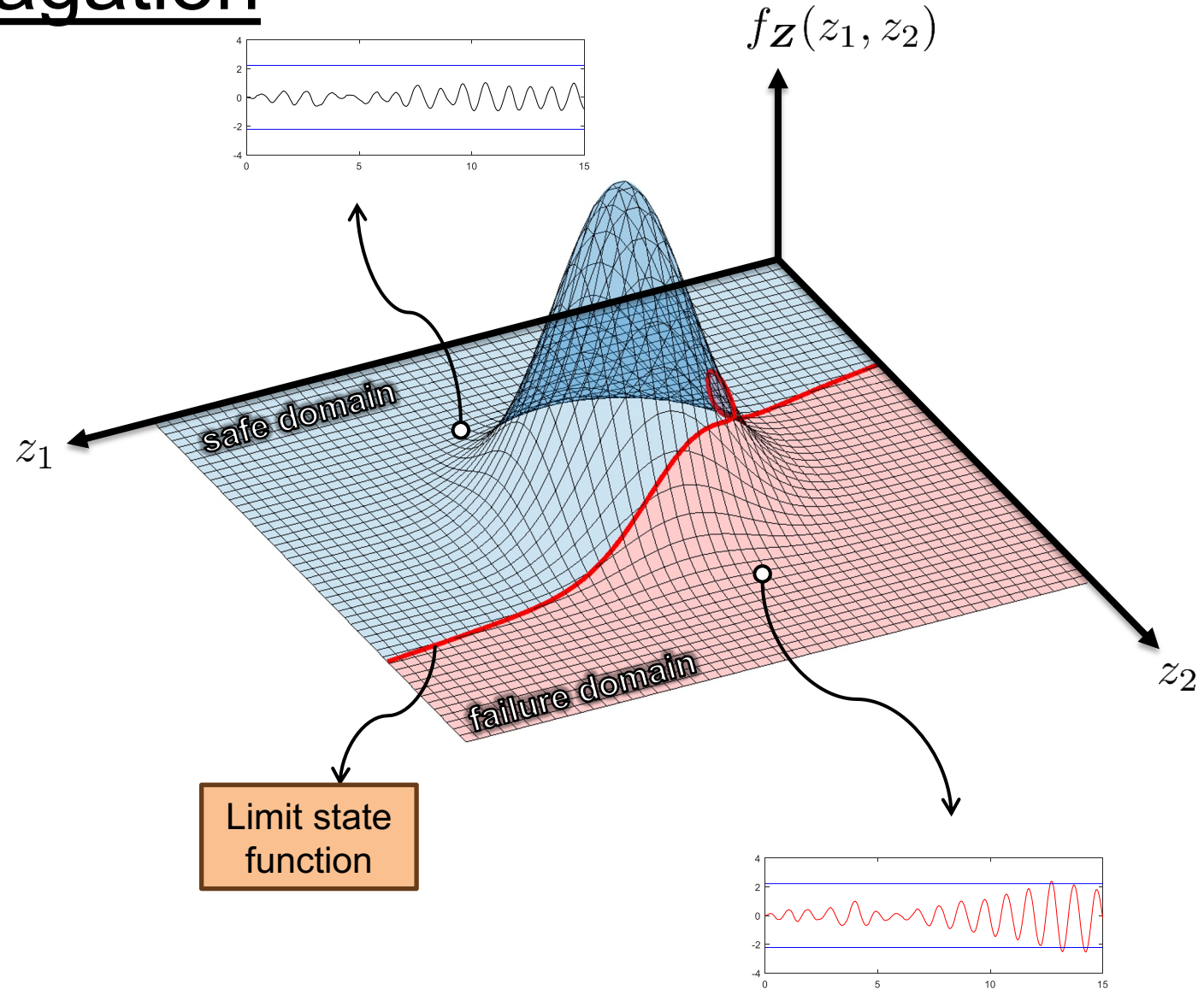
Design variables vector

Of interest: first excursion probability:

$$p_F = \int_{\mathbf{z} \in \mathbb{R}^{n_D}} I_F(\mathbf{y}, \mathbf{z}) f_Z(\mathbf{z}) d\mathbf{z}$$

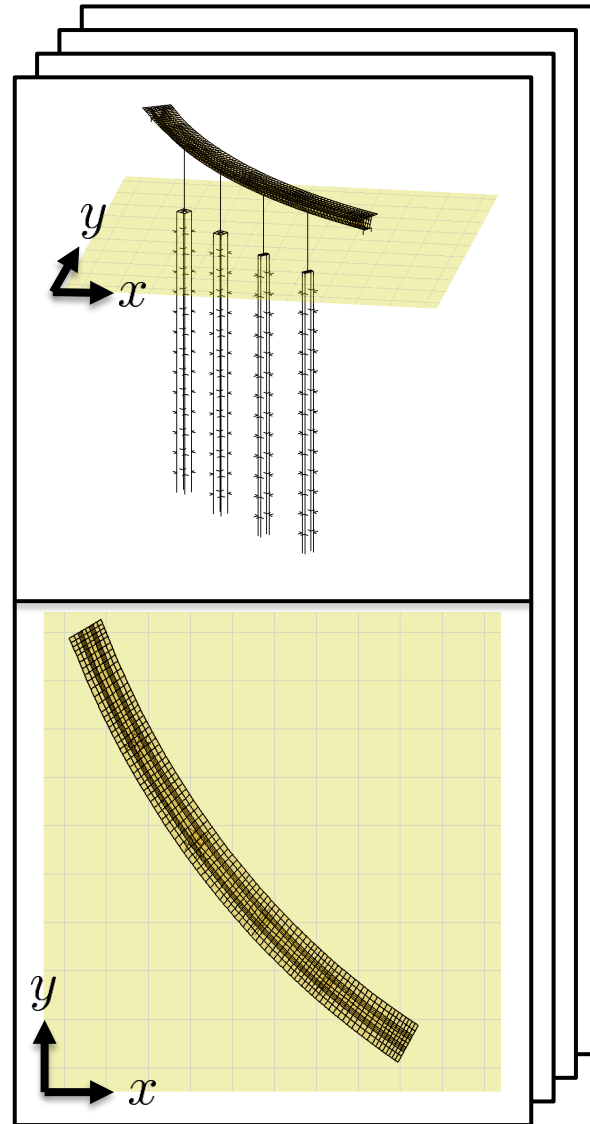
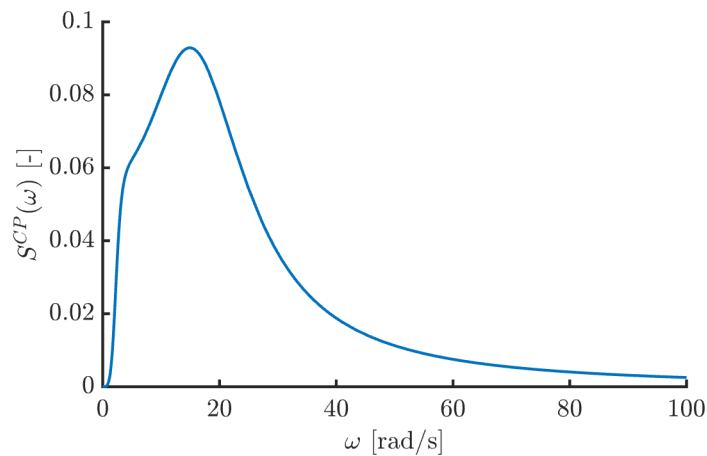
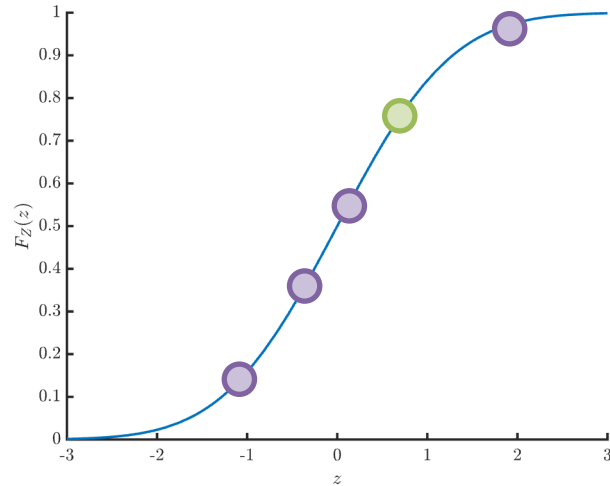
Indicator function

PDF, excitation



Limit state function

Reliability analysis

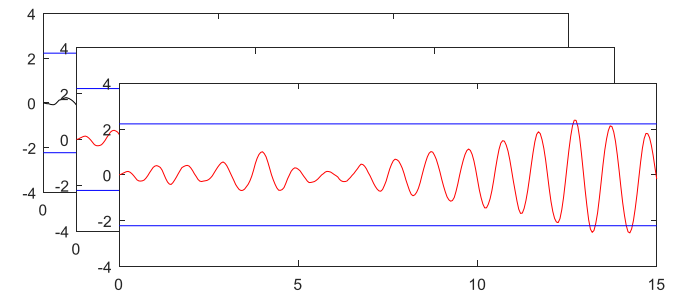


Aleatory

p_F

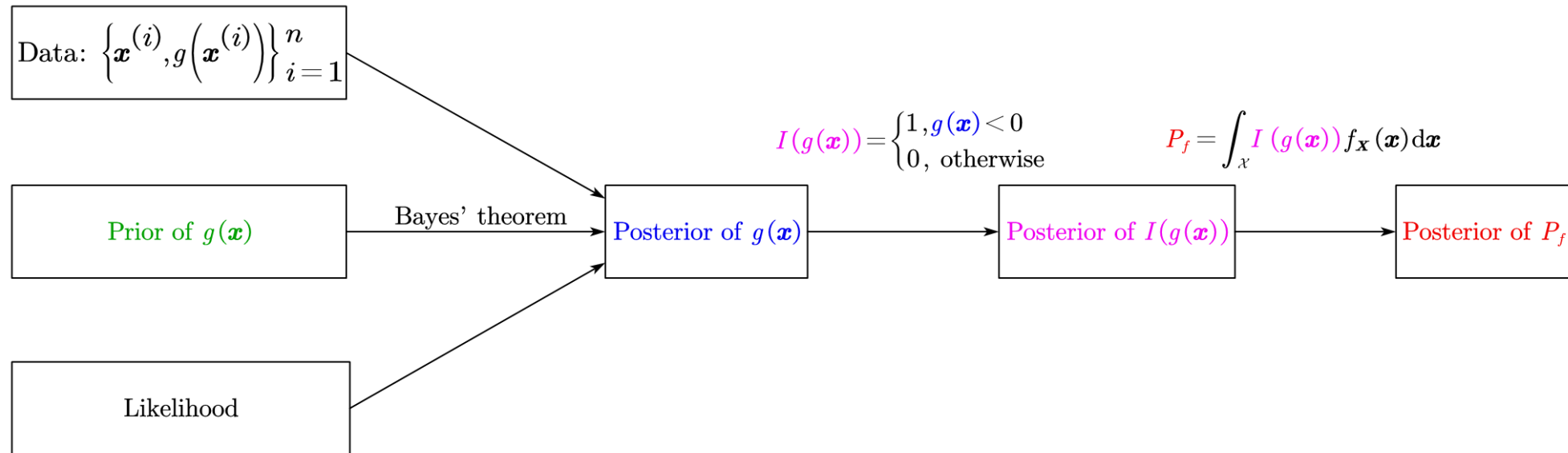
**Deterministic
model**

$\eta(t)$



$$p_F = \int_{\mathbf{z} \in \mathbb{R}^{n_D}} I_F(\mathbf{y}, \mathbf{z}) f_{\mathbf{Z}}(\mathbf{z}) d\mathbf{z}$$

Bayesian active learning



Step 3: Bayesian active learning of the failure probability

Idea	Method	Stopping Criterion	Learning function
Using the posterior mean	PBALQ [1]	$\frac{\int_{\mathcal{X}} \left[\Phi\left(-\frac{m_{g_n}(\mathbf{x})}{\sigma_{g_n}(\mathbf{x})}\right) - \Phi\left(-\frac{m_{g_n}(\mathbf{x})}{\sigma_{g_n}(\mathbf{x})} - b\right) \right] f_{\mathbf{X}}(\mathbf{x}) d\mathbf{x}}{\int_{\mathcal{X}} \Phi\left(-\frac{m_{g_n}(\mathbf{x})}{\sigma_{g_n}(\mathbf{x})}\right) f_{\mathbf{X}}(\mathbf{x}) d\mathbf{x}} < \epsilon$	$LF(\mathbf{x}) = \left[\Phi\left(-\frac{m_{g_n}(\mathbf{x})}{\sigma_{g_n}(\mathbf{x})}\right) - \Phi\left(-\frac{m_{g_n}(\mathbf{x})}{\sigma_{g_n}(\mathbf{x})} - b\right) \right] f_{\mathbf{X}}(\mathbf{x})$
Using the posterior variance also, but with simplification	QBALC [2]	$\frac{\sqrt{\bar{\rho}} \int_{\mathcal{X}} \sqrt{\Phi\left(-\frac{m_{g_n}(\mathbf{x})}{\sigma_{g_n}(\mathbf{x})}\right) \Phi\left(\frac{m_{g_n}(\mathbf{x})}{\sigma_{g_n}(\mathbf{x})}\right)} f_{\mathbf{X}}(\mathbf{x}) d\mathbf{x}}{\int_{\mathcal{X}} \Phi\left(-\frac{m_{g_n}(\mathbf{x})}{\sigma_{g_n}(\mathbf{x})}\right) f_{\mathbf{X}}(\mathbf{x}) d\mathbf{x}} < \epsilon$	$LF(\mathbf{x}; p) = \sqrt{\Phi\left(-\frac{m_{g_n}(\mathbf{x})}{p\sigma_{g_n}(\mathbf{x})}\right) \Phi\left(\frac{m_{g_n}(\mathbf{x})}{p\sigma_{g_n}(\mathbf{x})}\right)} f_{\mathbf{X}}(\mathbf{x})$
	WBALC [3]	$\frac{\hat{\lambda}_{\hat{I}_n}}{\hat{m}_{\hat{P}_{f,n}}} < \epsilon$	$LF(\mathbf{u}) = \sigma_{\tilde{g}_n}(\mathbf{u}) \Phi\left(-\frac{m_{\tilde{g}_n}(\mathbf{u})}{\sigma_{\tilde{g}_n}(\mathbf{u})}\right) \Phi\left(\frac{m_{\tilde{g}_n}(\mathbf{u})}{\sigma_{\tilde{g}_n}(\mathbf{u})}\right) \phi(\mathbf{u})$

[1] Dang, Chao, Matthias G.R. Faes, Marcos A. Valdebenito, Pengfei Wei, and Michael Beer. "Partially Bayesian Active Learning Cubature for Structural Reliability Analysis with Extremely Small Failure Probabilities." *Computer Methods in Applied Mechanics and Engineering* 422 (March 2024): 116828.

[2] Dang, Chao, Alice Cicirello, Marcos A. Valdebenito, Matthias G.R. Faes, Pengfei Wei, and Michael Beer. "Structural Reliability Analysis with Extremely Small Failure Probabilities: A Quasi-Bayesian Active Learning Method." *Probabilistic Engineering Mechanics* 76 (April 2024): 103613.

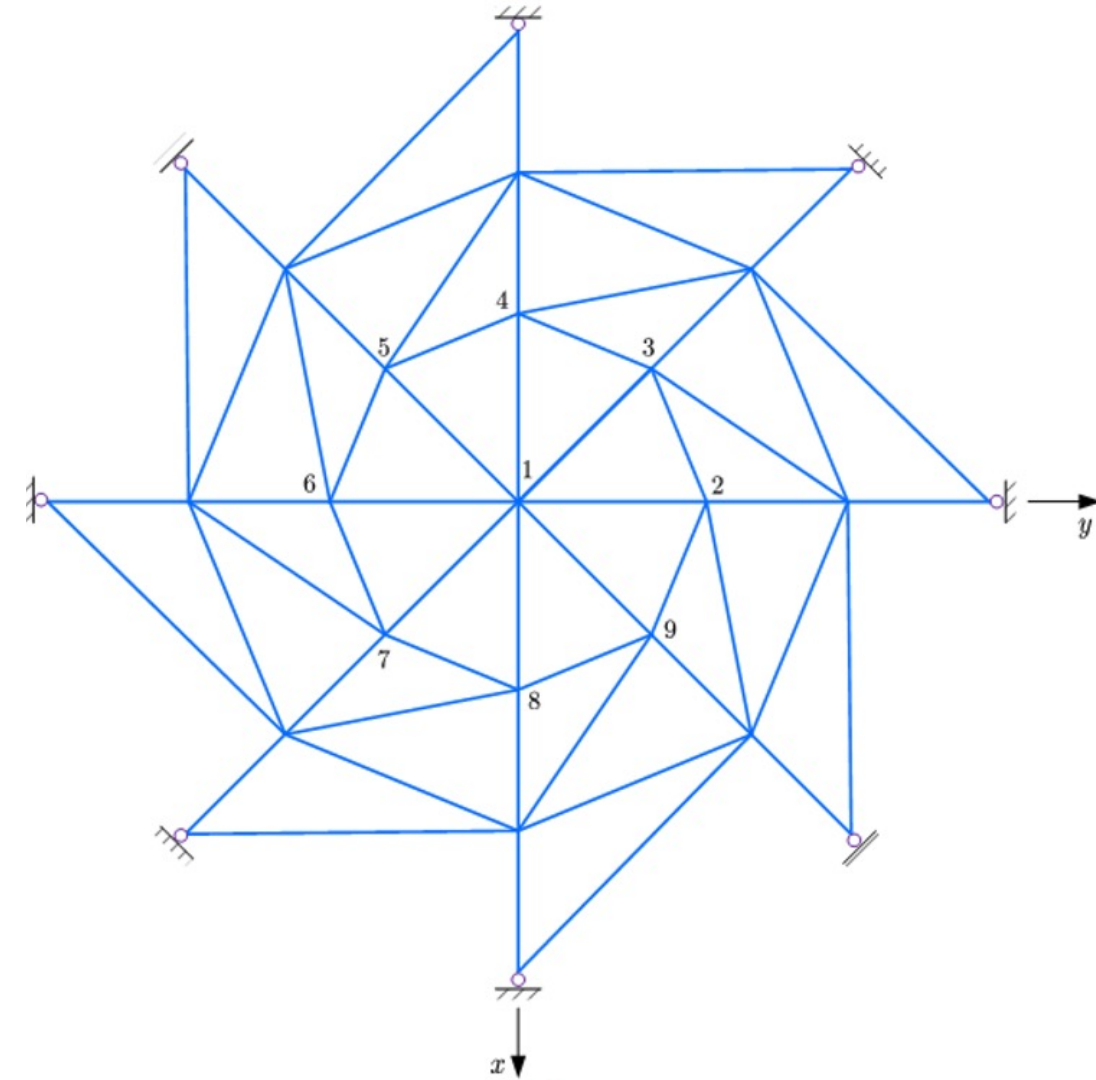
[3] Dang, Chao, Tong Zhou, Marcos A. Valdebenito, and Matthias G.R. Faes. "Yet Another Bayesian Active Learning Reliability Analysis Method." *Structural Safety* 112 (January 2025): 102539.

An example: a 56-bar truss structure

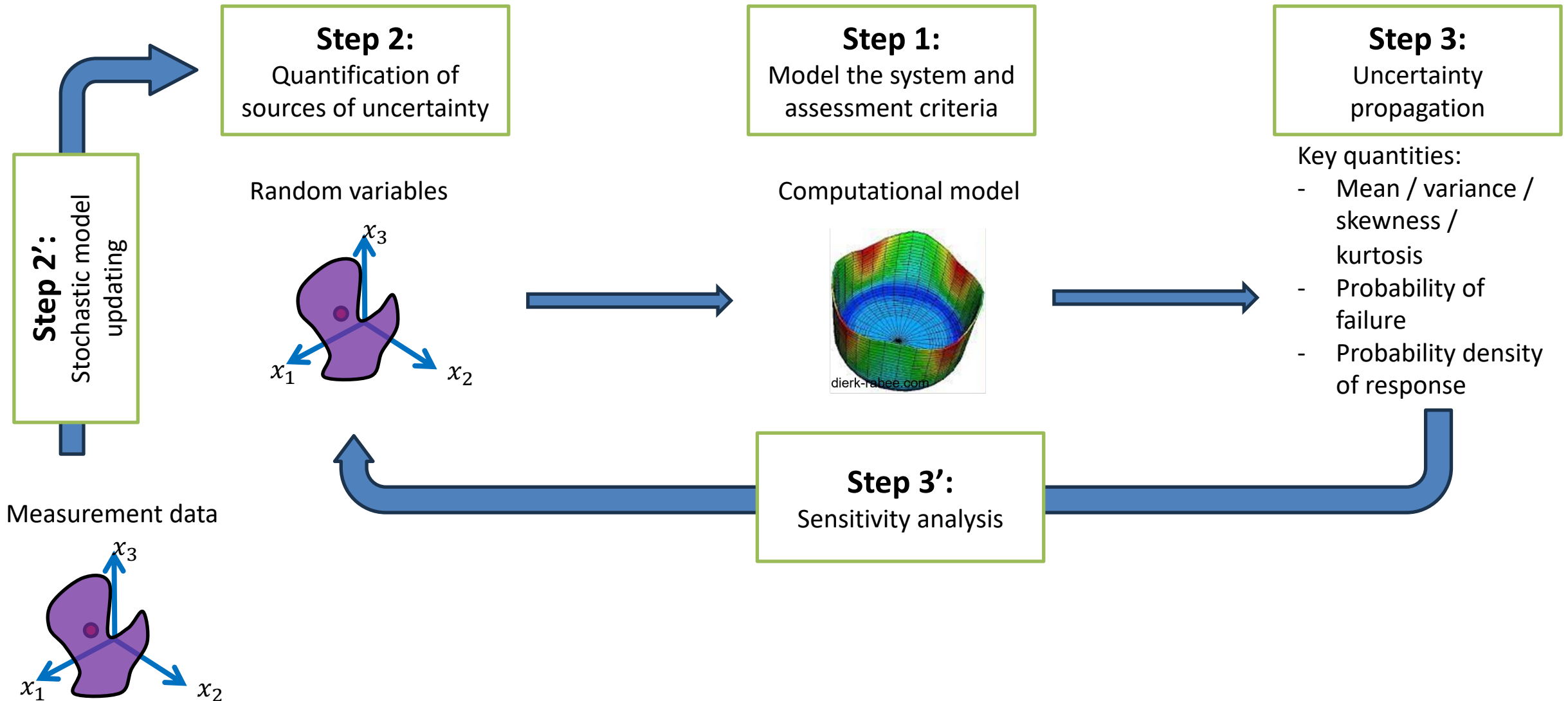


$$g(P_1, P_2, \dots, P_9, E, A) = \Delta - V_1(P_1, P_2, \dots, P_9, E, A),$$

Method	ε	N_{call}	$\hat{P}_f$	$\delta \hat{P}_f$
IS	—	66,107	$4.94 \cdot 10^{-8}$	1.00%
AK-MCMC	—	465.00	$4.97 \cdot 10^{-8}$	2.92%
PBALC	$\varepsilon_2 = 5.00\%$	26.90	$4.85 \cdot 10^{-8}$	4.61%
SBALQ	$\varepsilon = 4.00\%$	31.40	$4.77 \cdot 10^{-8}$	5.32%
QBALC	$\varepsilon = 5.00\%$	29.20	$4.69 \cdot 10^{-8}$	6.42%
WBALQ	$\varepsilon = 4.00\%$	26.30	$4.87 \cdot 10^{-8}$	5.57%



General uncertainty quantification overview



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We are always happy to host guests from other groups to set-up and maintain joint collaborations, as well as to support the application of CSC and Humboldt Fellowships.