

Using FEMU for identifying plastic material behavior of heavy gauge steel

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Material Twin Bridge*

MT1.0 facilitates understanding material behavior



MT1.0

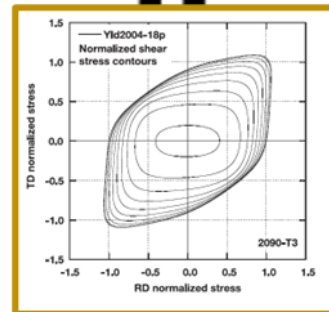
**Real
Material
Behavior**



**Virtual
Material
Behavior**



Experimental
Mechanics



Material
Modelling



Calibration
Methods

* After an idea of prof. M. Halilović

Material Twin Bridge

MT2.0 facilitates crossing the material twin bridge faster/better

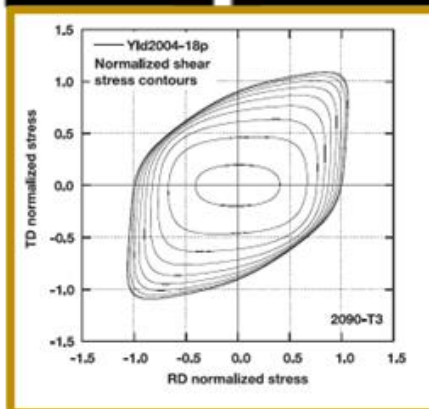


MT2.0

**Real
Material
Behavior**



**Virtual
Material
Behavior**



Material
Modelling



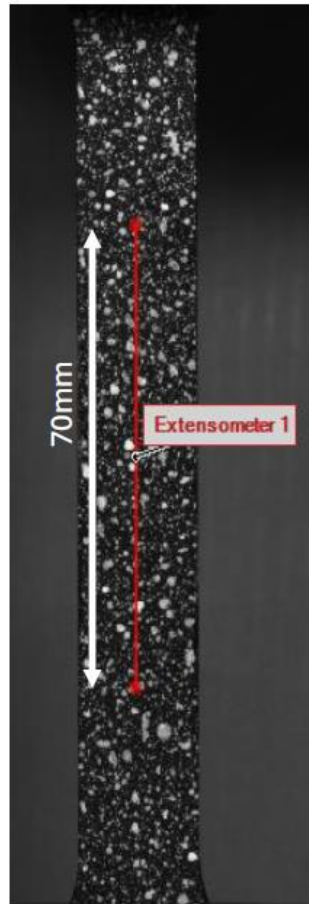
Experimental
Mechanics



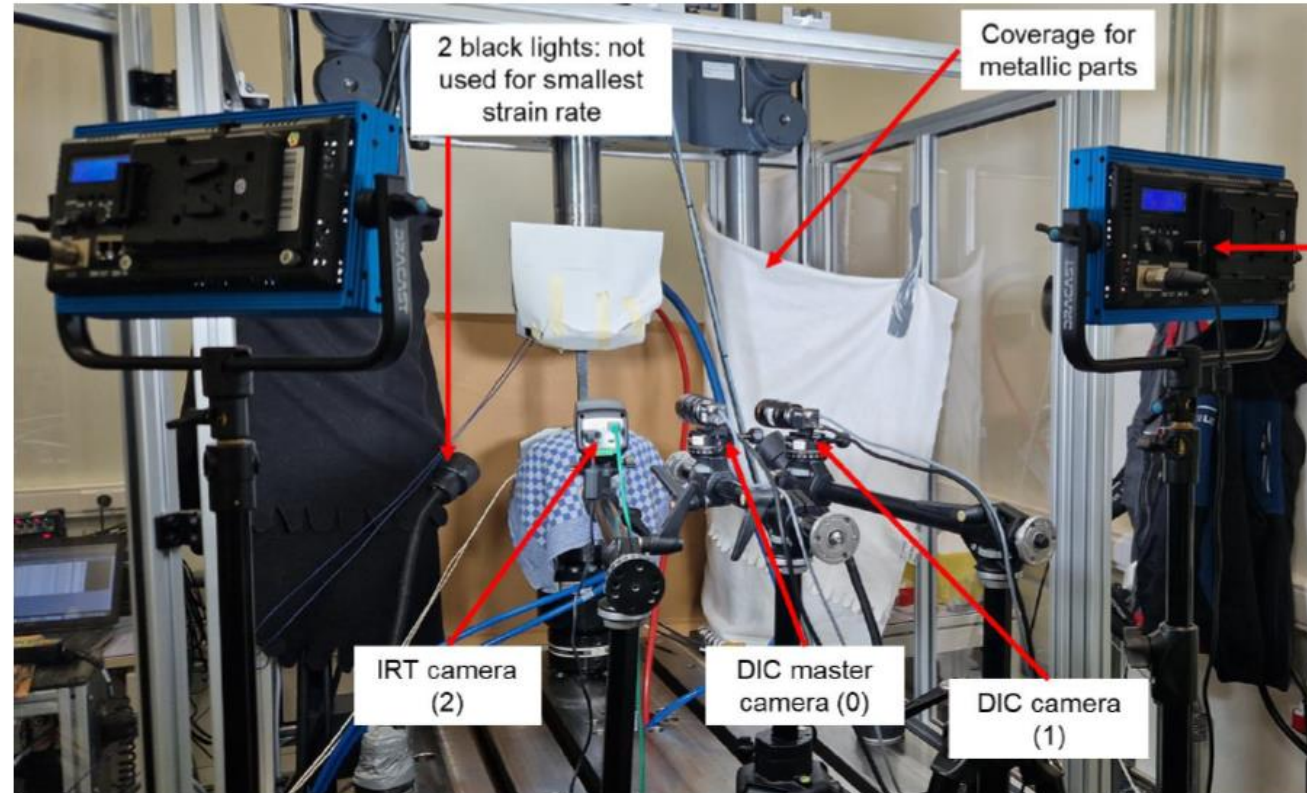
Inverse
Methods



MT1.0



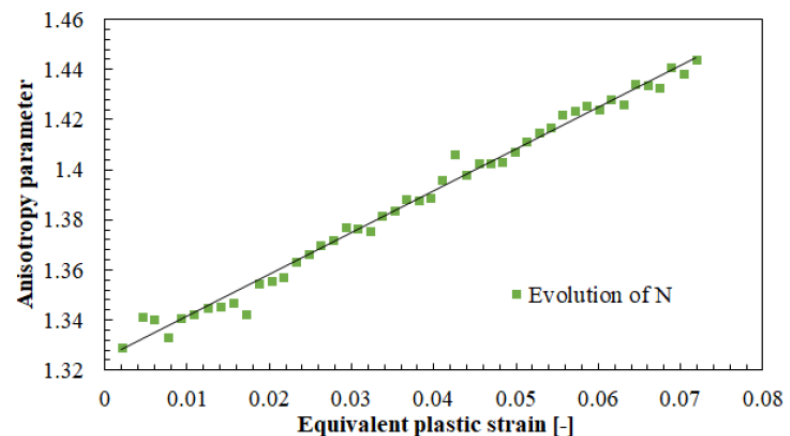
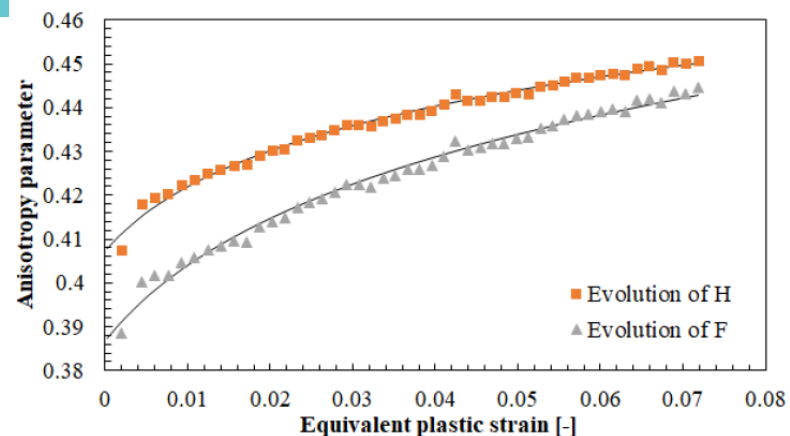
Tensile testing using combined IRT-DIC



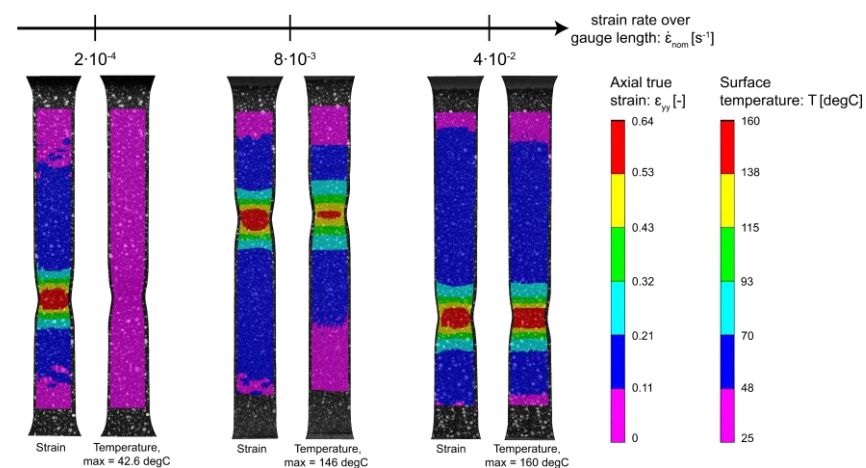
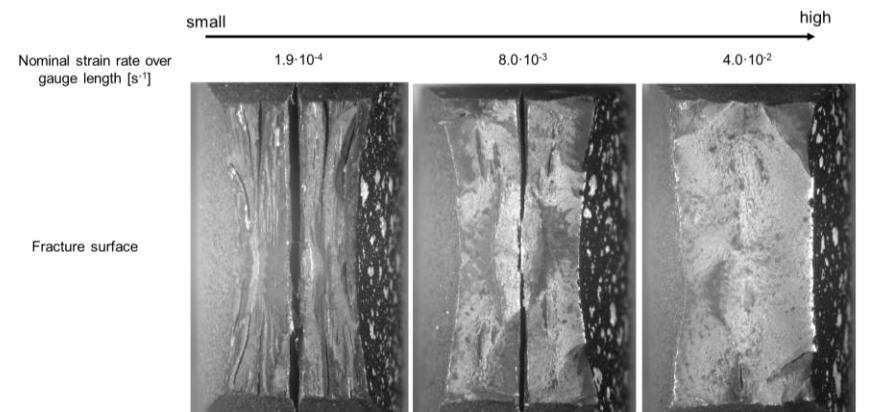


MT1.0

Evolution of anisotropy parameters



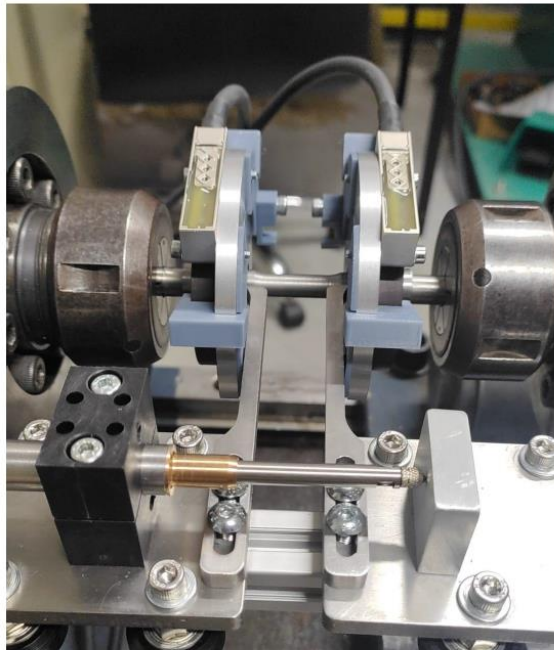
Onset of damage in relation to strain rate and temperature



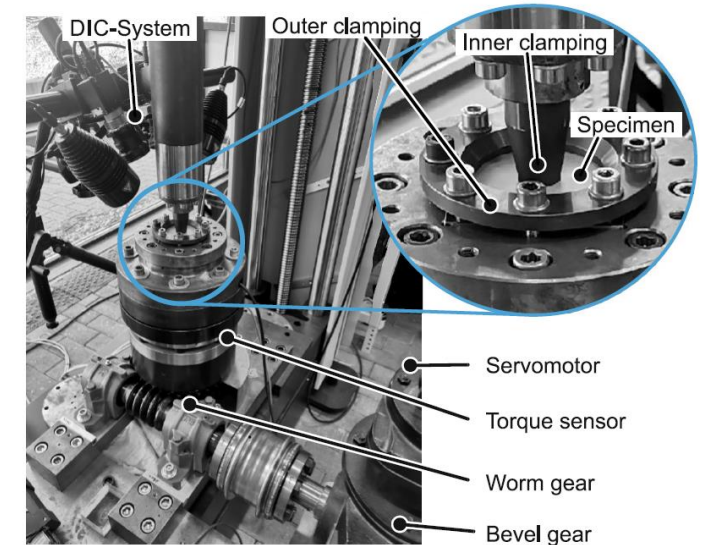
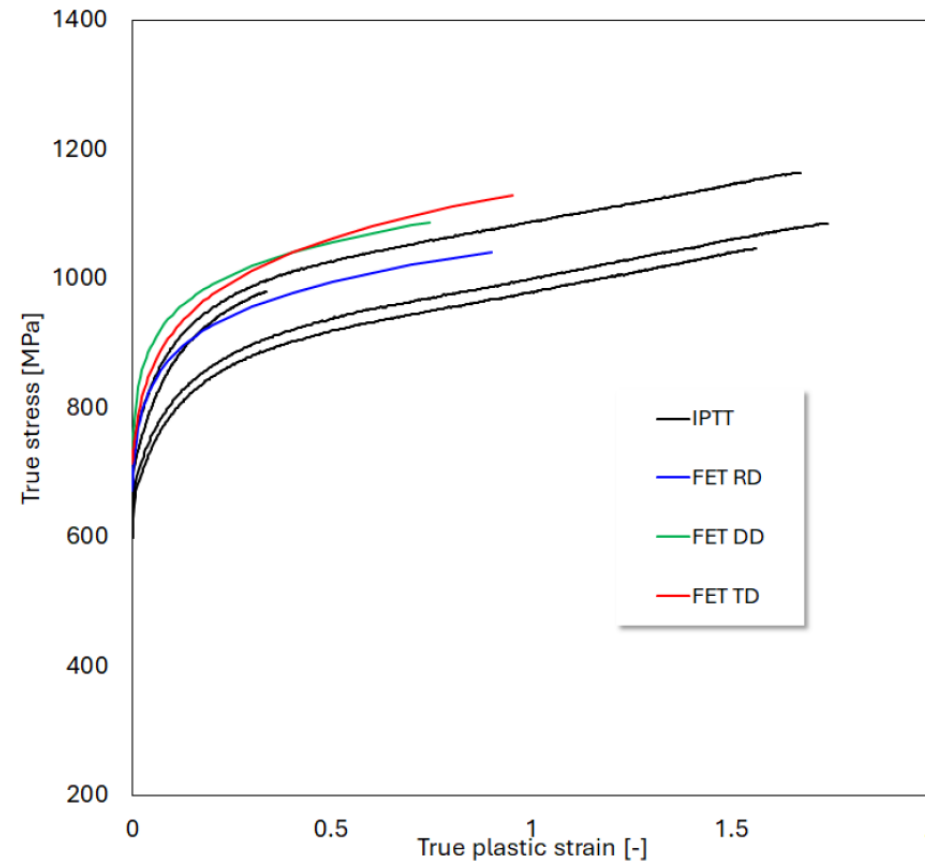


MT1.0

More advanced experiments enabling to probe a specific material response



Free-End Torsion Test (FET)



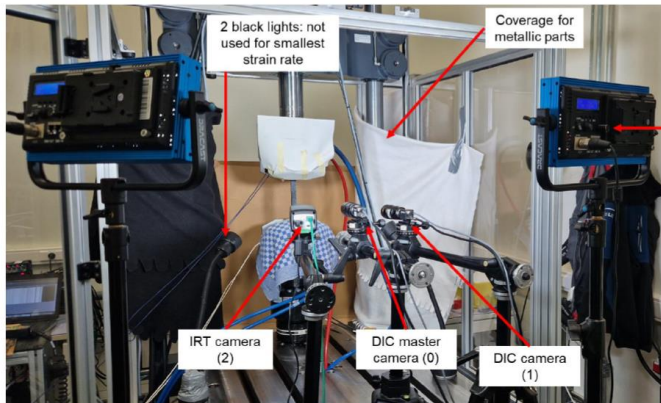
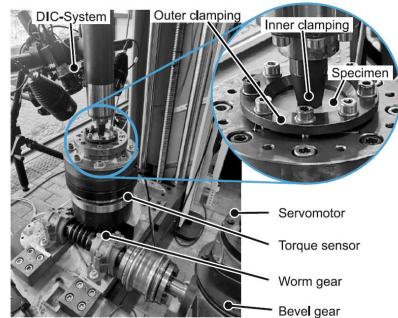
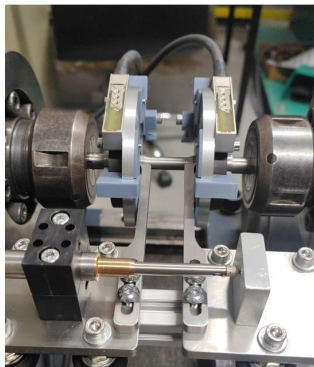
The in-plane torsion test (IPPT)

Material Twin Bridge



MT1.0

blueprint of material behavior



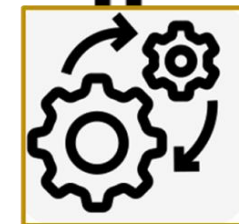
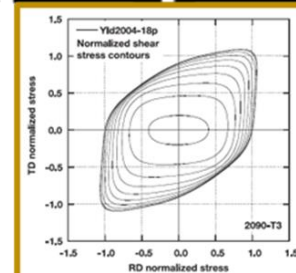
MT2.0

crossing the material twin bridge faster/better (for a specific material response in relation to an application)

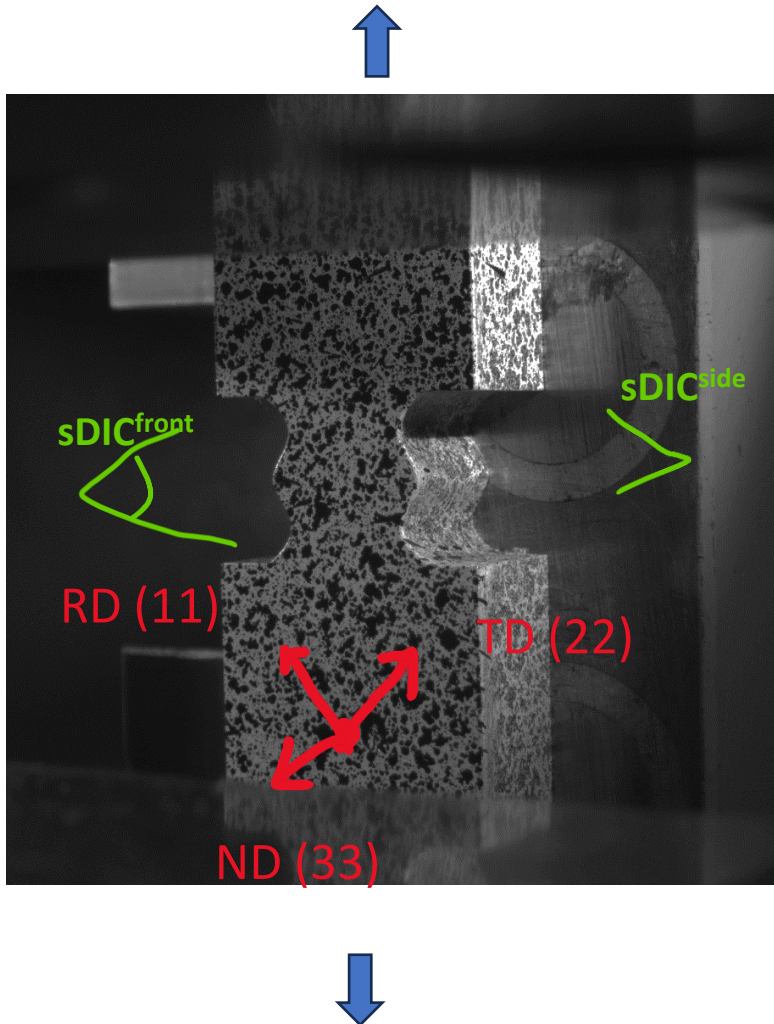
Real
Material
Behavior



Virtual
Material
Behavior



Material Phenomenology: anisotropic yielding



Material S700MC, nominal thickness 12 mm

Known: average strain hardening behavior in RD

Unknown: 5 anisotropy parameters of 3D Hill48 ($G + H = 1$)

$$\sigma_{eq}^2 = F(\sigma_{22} - \sigma_{33})^2 + G(\sigma_{33} - \sigma_{11})^2 + H(\sigma_{11} - \sigma_{22})^2 + 2L\sigma_{23}^2 + 2M\sigma_{31}^2 + 2N\sigma_{12}^2$$

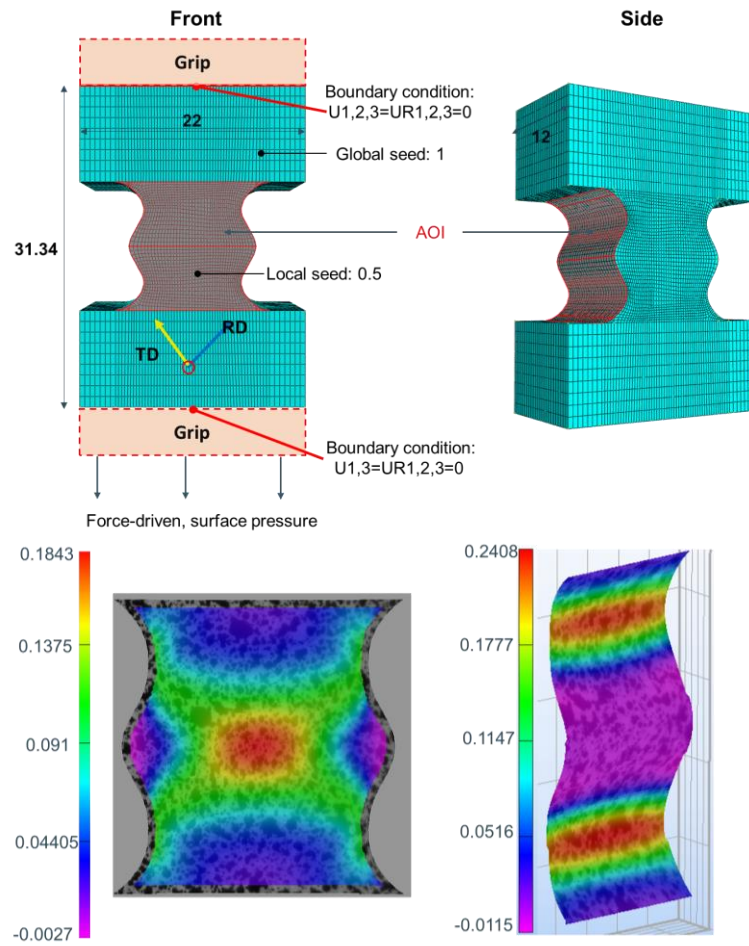
FEMU: Strain-based cost function

$$C(\mathbf{p}) = C(\mathbf{p})^{Front} + C(\mathbf{p})^{side}$$

$$C(\mathbf{p})^{side} = \sum_{i=1}^m \sum_{j=1}^{n_i} \delta \left[\left(\frac{\epsilon_{yy,ij}^{exp} - \epsilon_{yy,ij}^{num}}{\epsilon_{yy,RMS,i}^{exp}} \right)^2 + \left(\frac{\epsilon_{zz,ij}^{exp} - \epsilon_{zz,ij}^{num}}{\epsilon_{zz,RMS,i}^{exp}} \right)^2 + \left(\frac{\epsilon_{yz,ij}^{exp} - \epsilon_{yz,ij}^{num}}{\epsilon_{yz,RMS,i}^{exp}} \right)^2 \right]$$

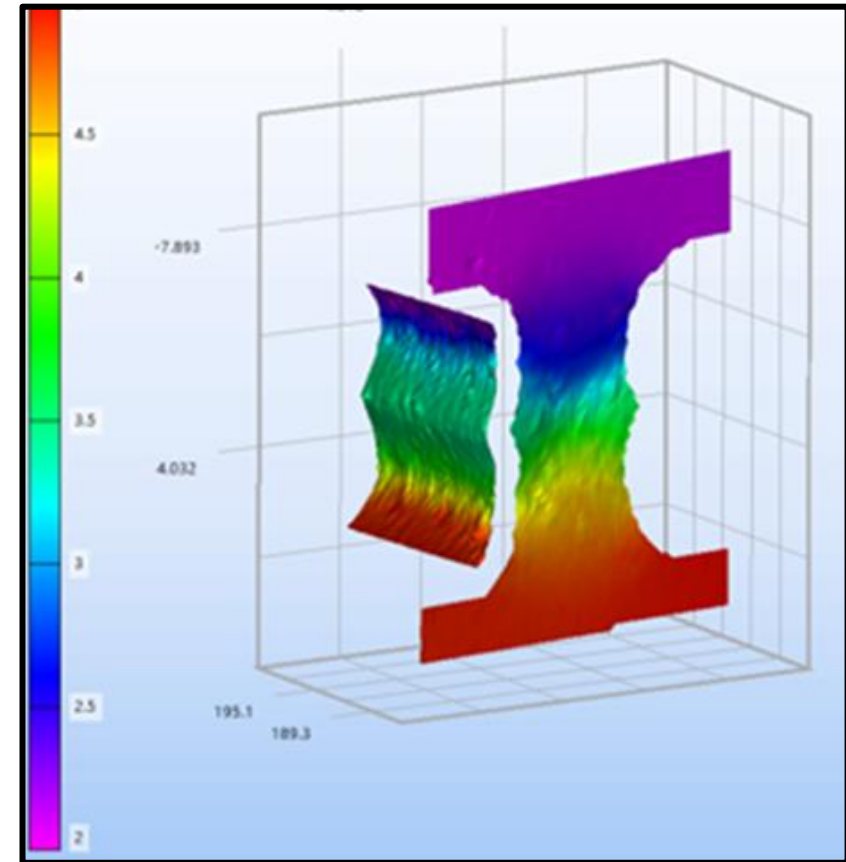
MT2.0: Specimen design

Shape optimization: maximizing strain heterogeneity



DVT

Stereo DIC front + Stereo DIC side



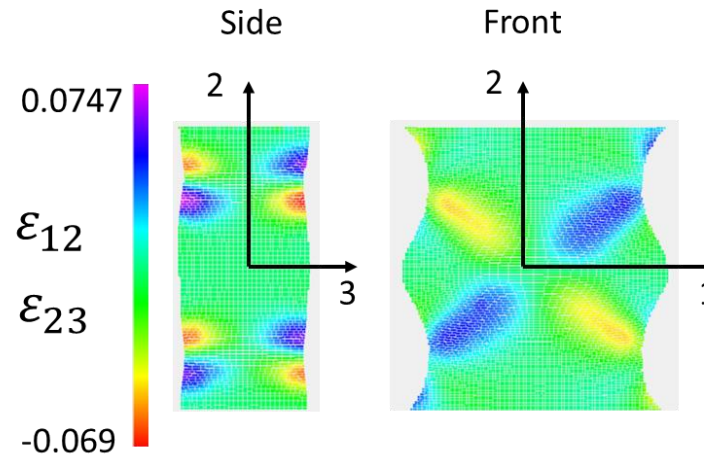
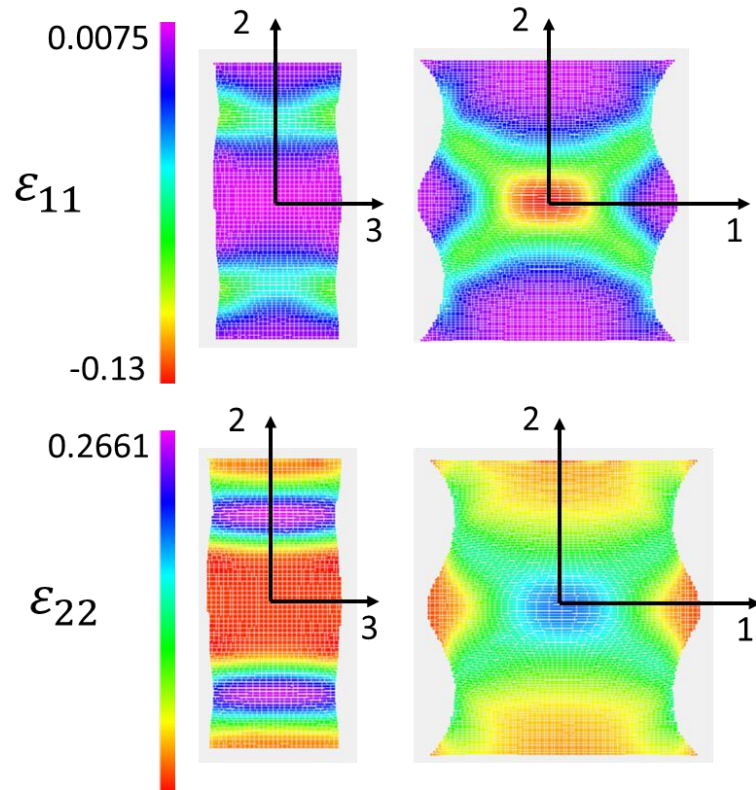
ϵ^{Mises}

Stereo DIC front

Stereo DIC side

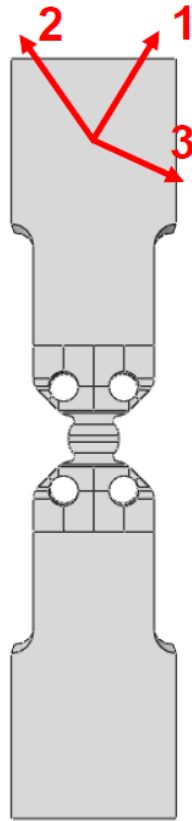
MT2.0: Specimen design

Shape optimization: maximizing strain heterogeneity

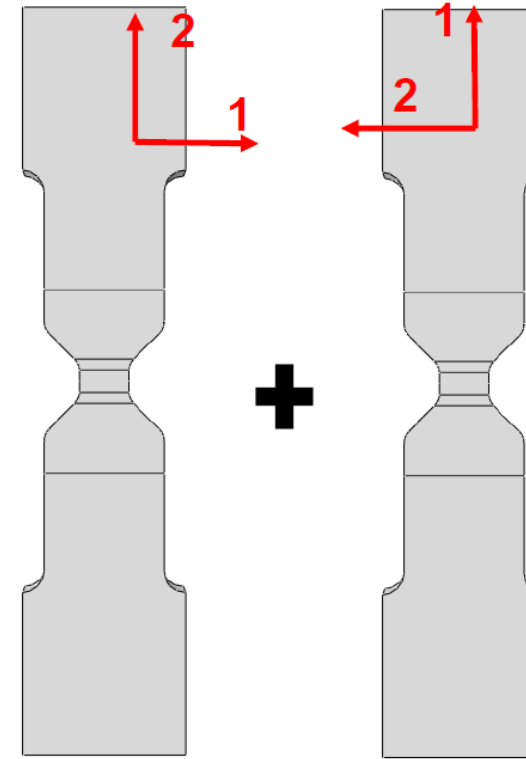


- Computationally heavy for thick specimens.
- Identifiability cannot be guaranteed.
- Material orientation should be a design variable.
- Spatial convergence of the measurement method ?

Identifiability analysis: maximizing parameter (set) identifiability



Single complex specimen approach

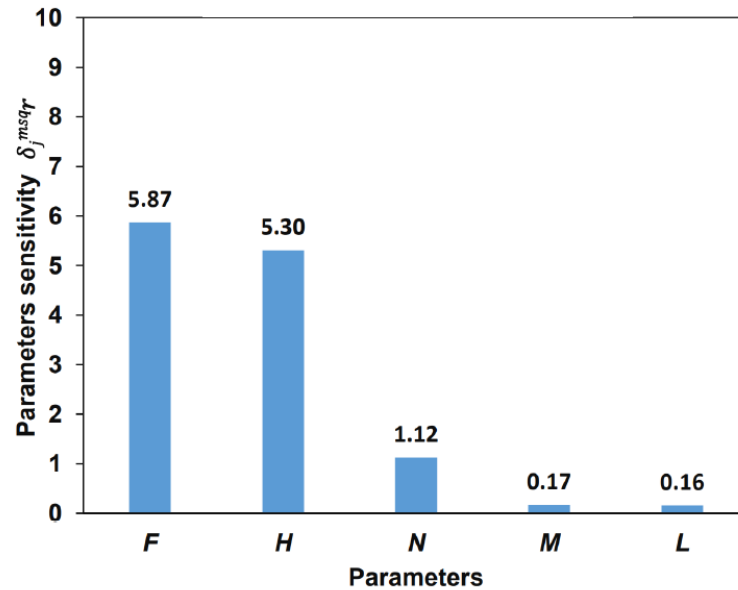


Two-specimen approach

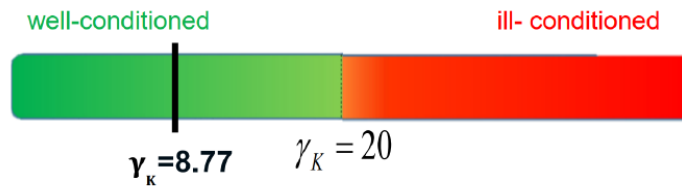
MT2.0: Specimen design

Identifiability analysis: maximizing parameter identifiability

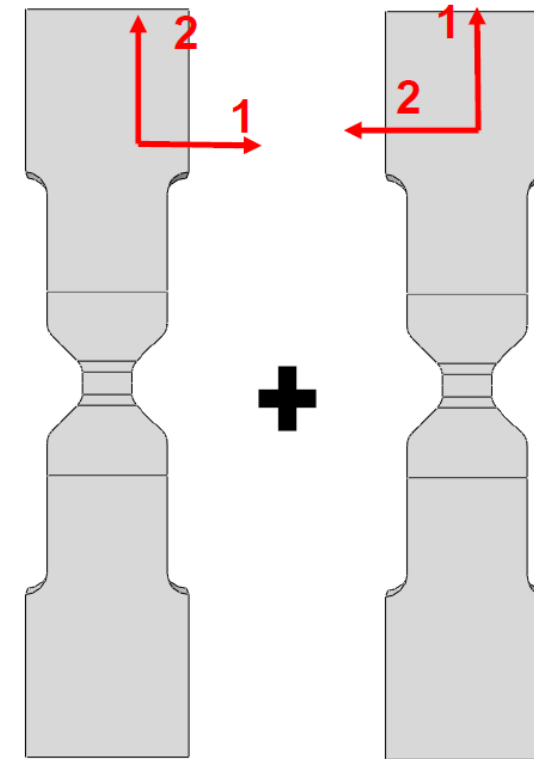
Sensitivity
Strength



Collinearity index



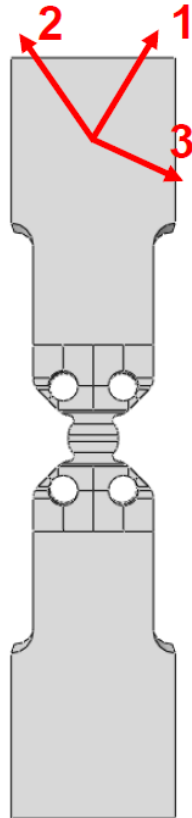
Identifiability analysis



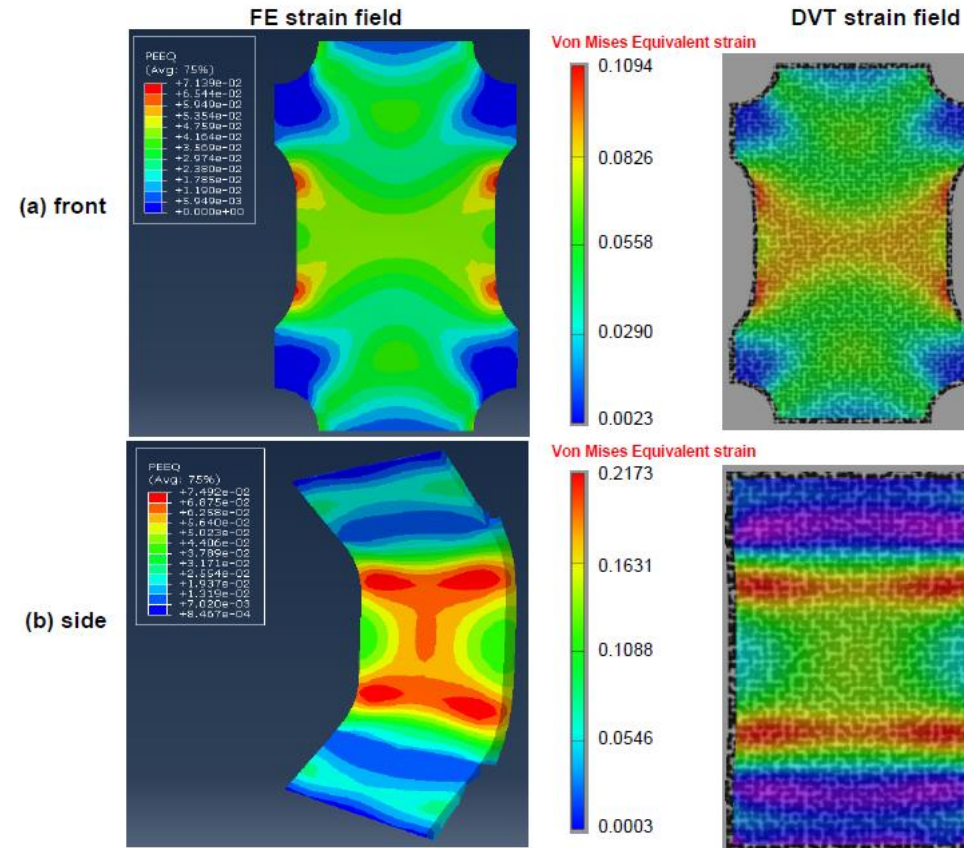
Two-specimen approach

MT2.0: Specimen design - DVT

Digital Virtual Twin to evaluate FEMU



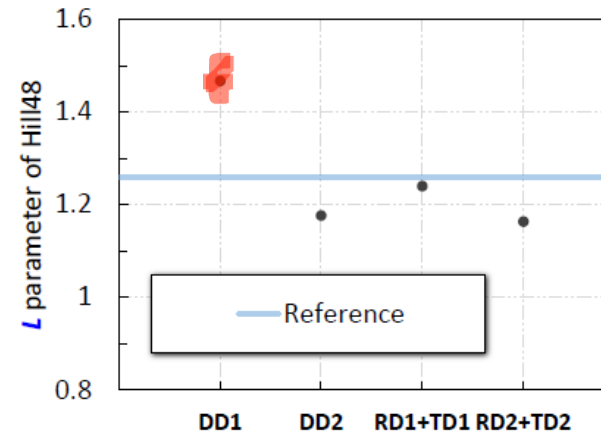
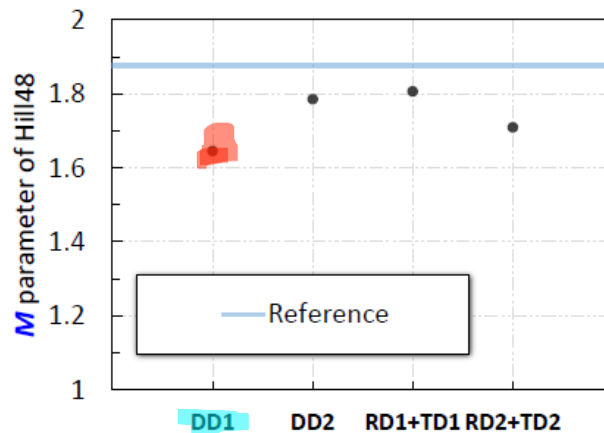
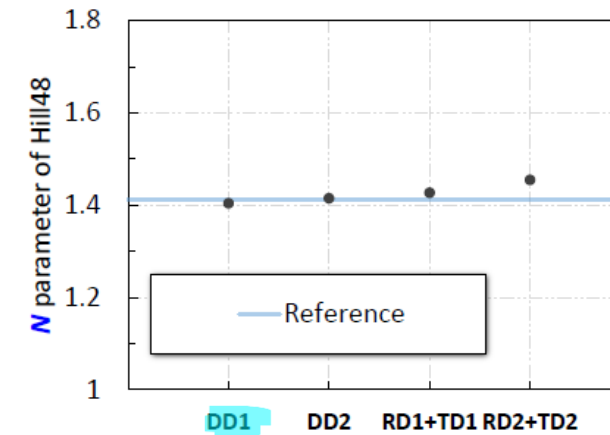
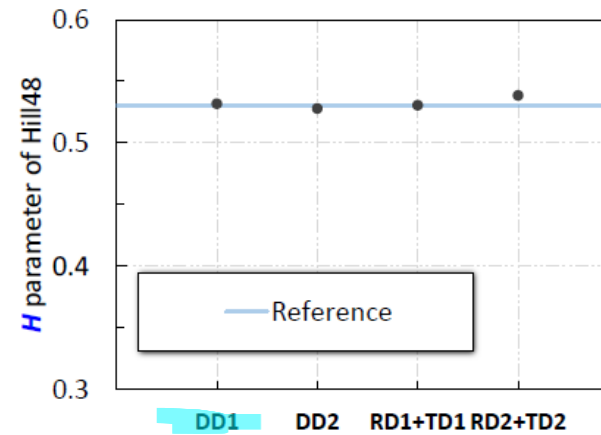
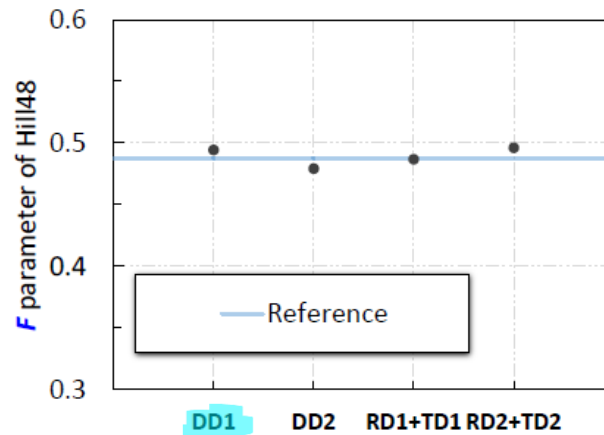
Single complex specimen approach



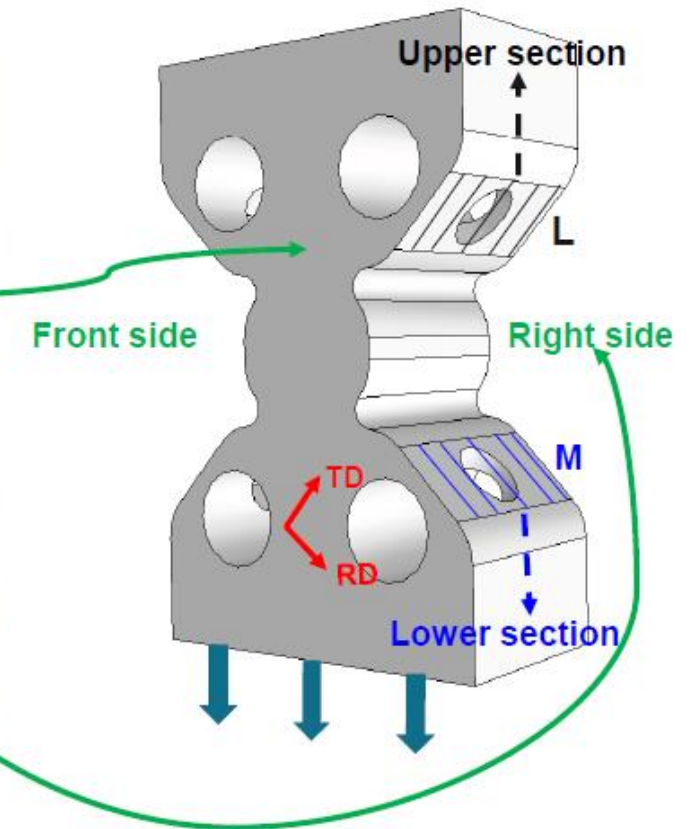
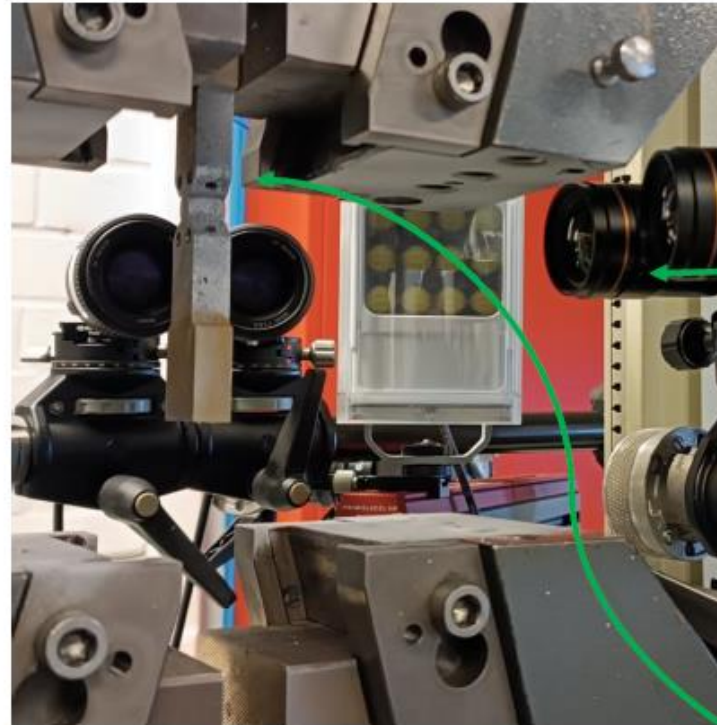
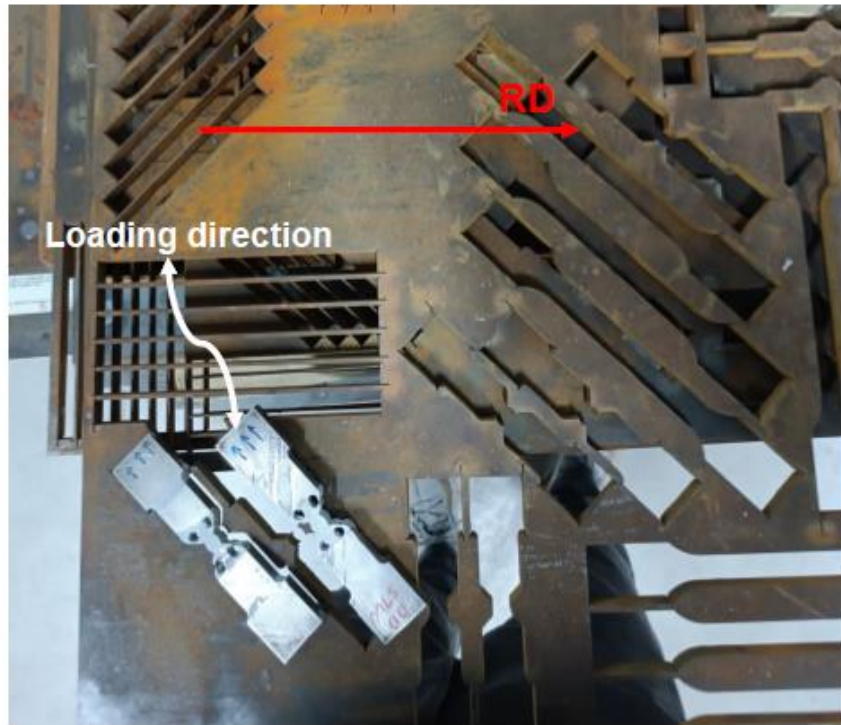
Metrological aspects

MT2.0: Specimen Design - DVT

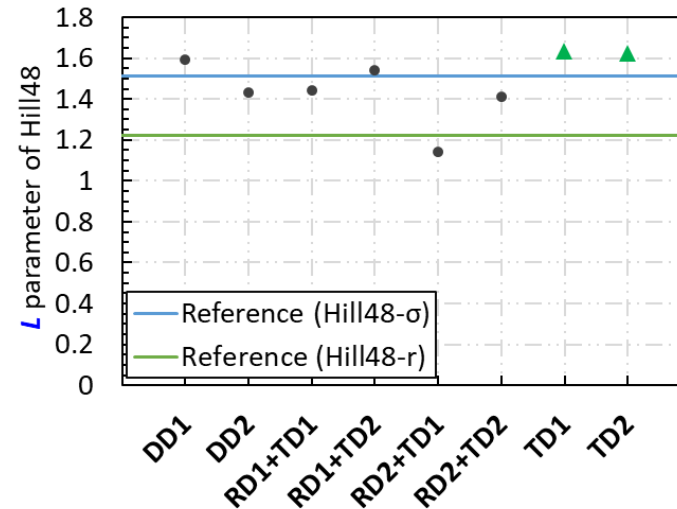
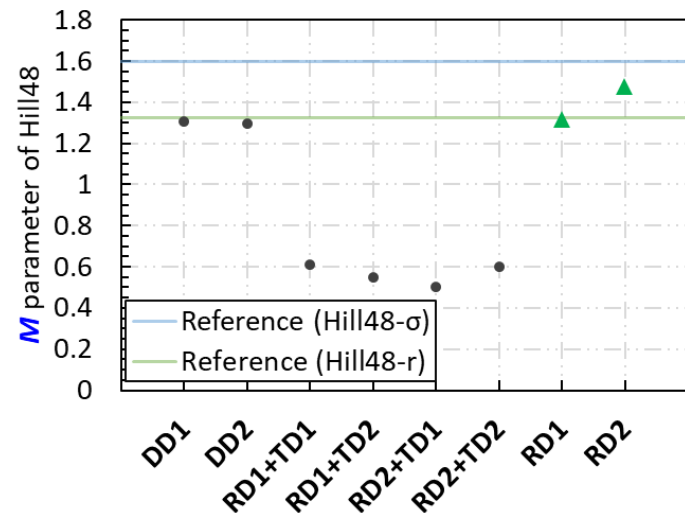
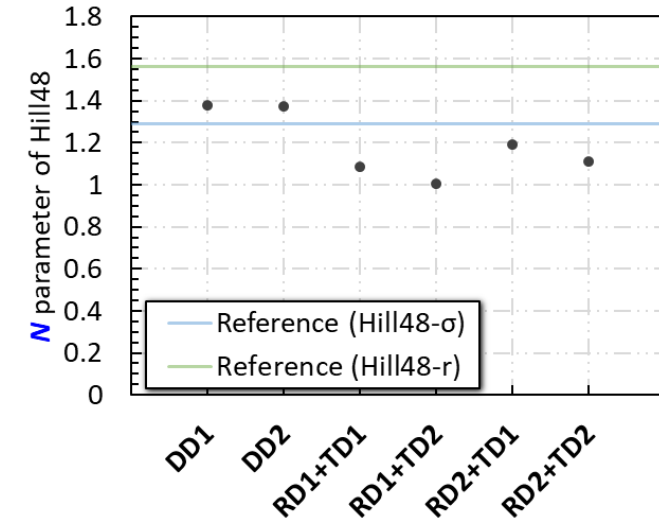
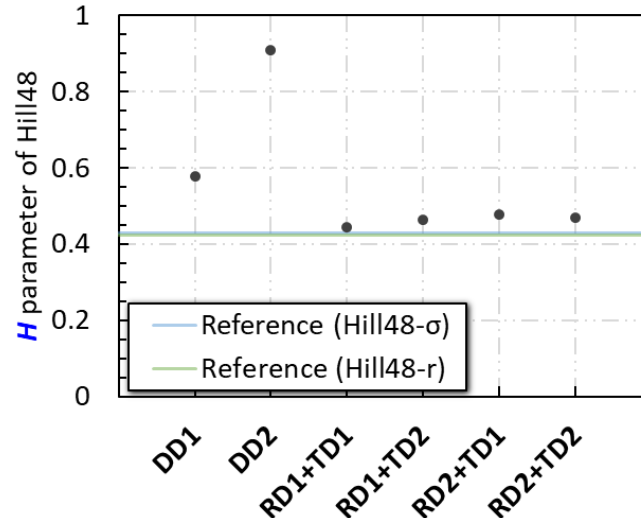
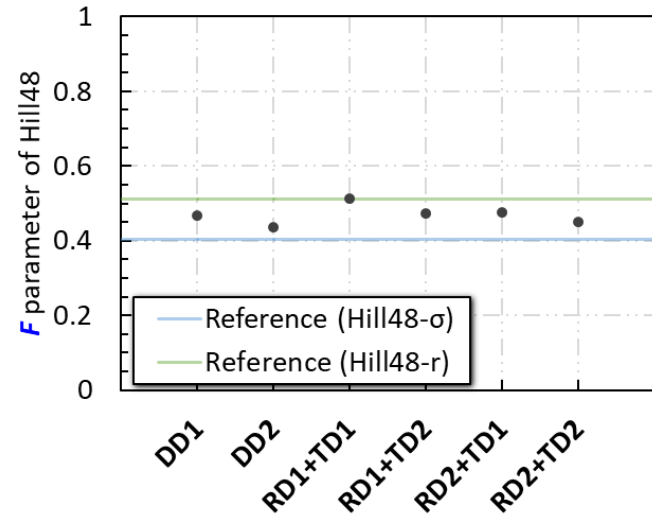
Digital Virtual Twin



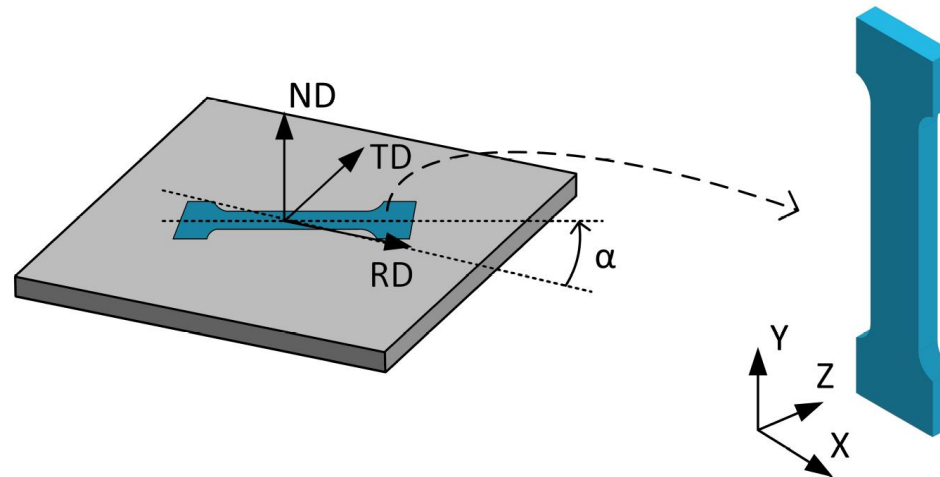
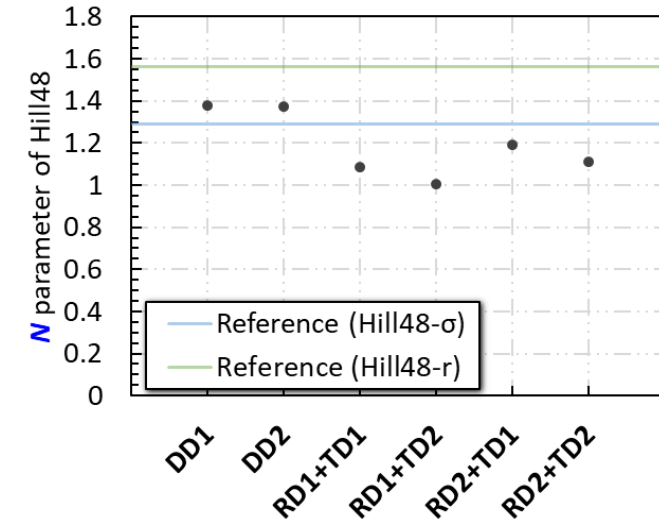
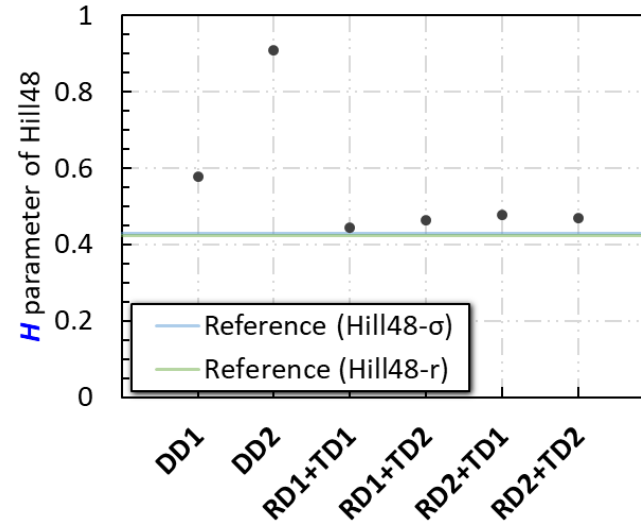
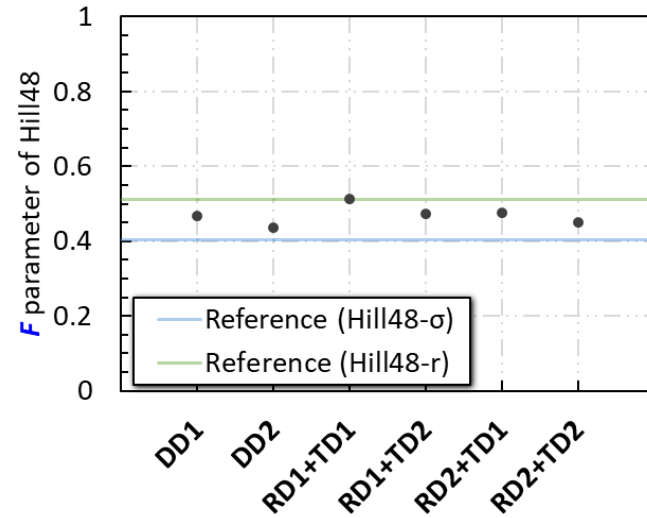
MT2.0: Experimental validation



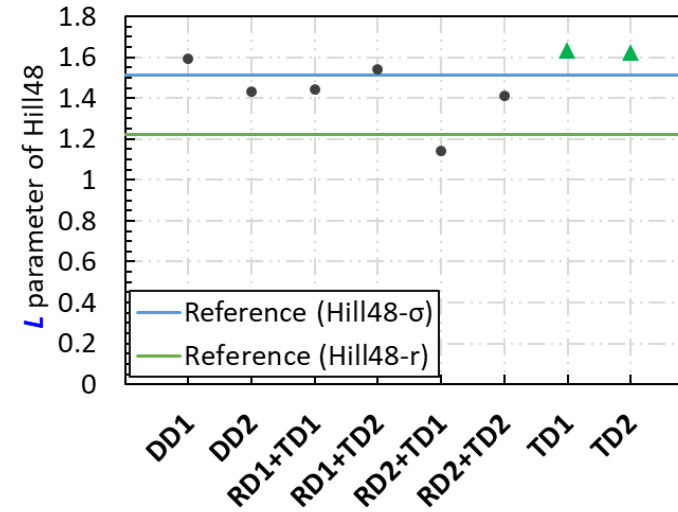
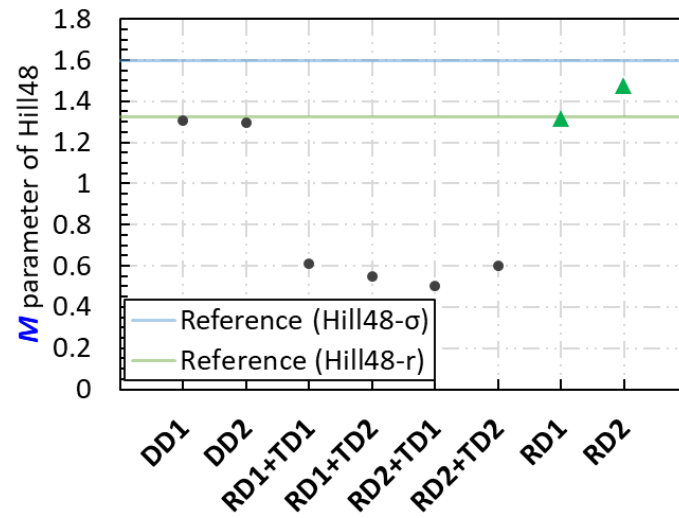
MT2.0: Experimental validation – “Reference” data



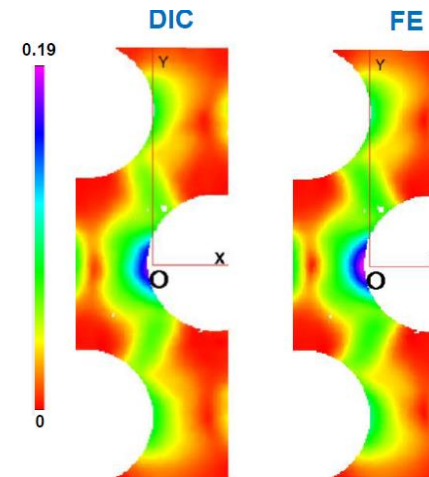
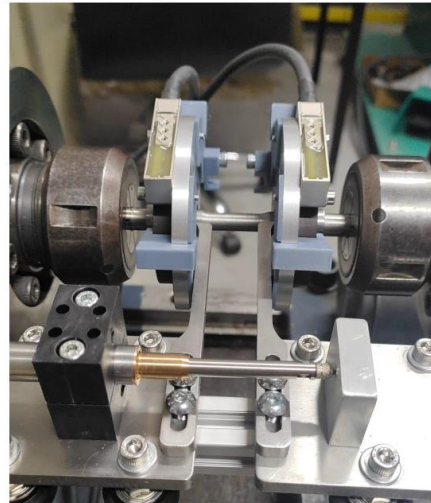
MT2.0: Experimental validation – “Reference” data



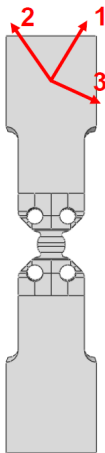
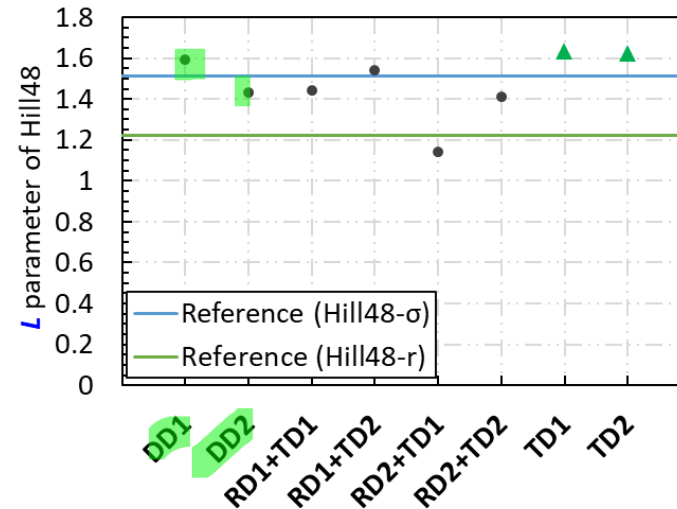
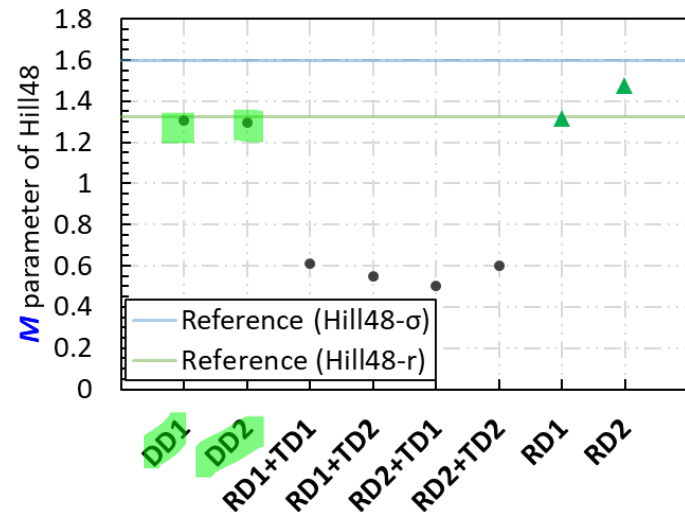
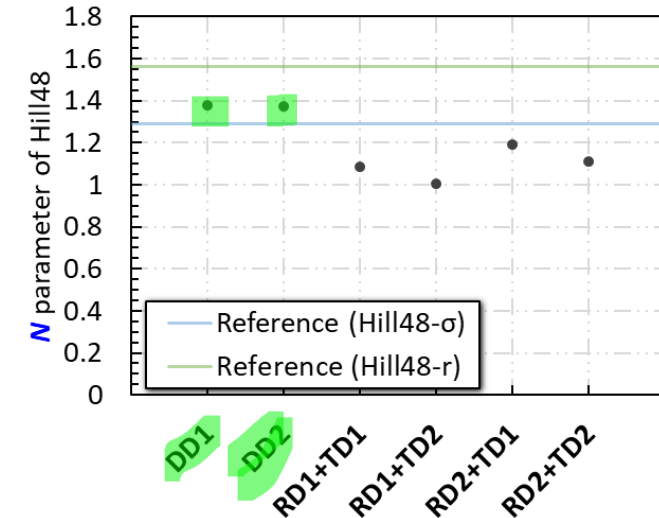
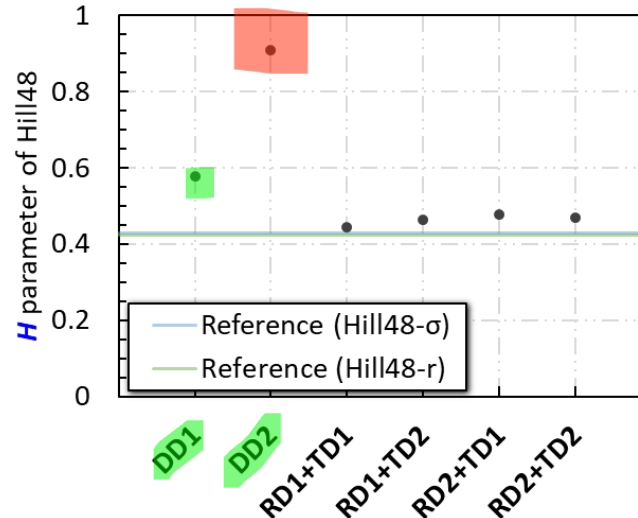
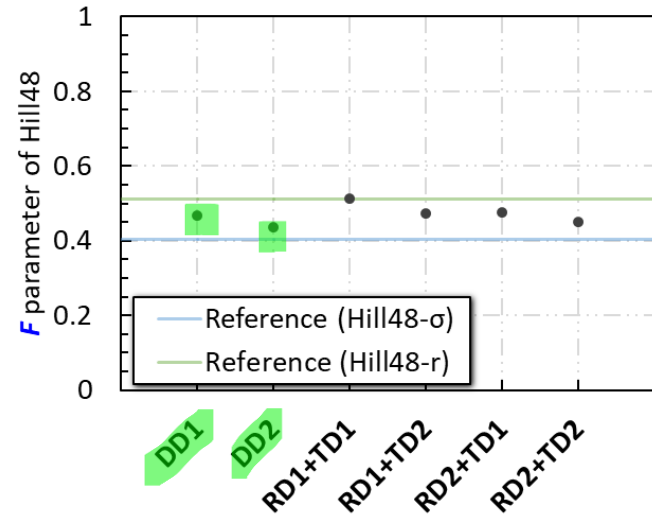
MT2.0: Experimental validation – “Reference” data



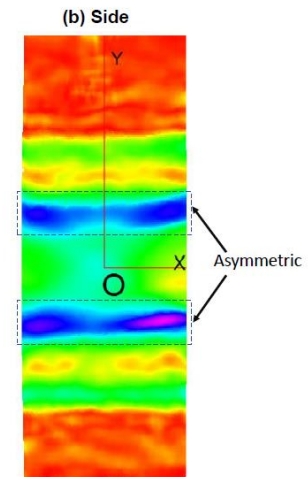
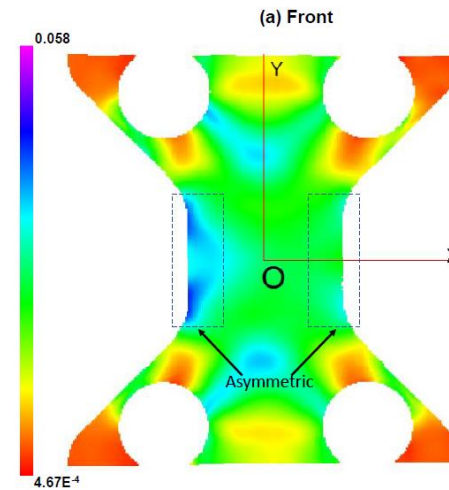
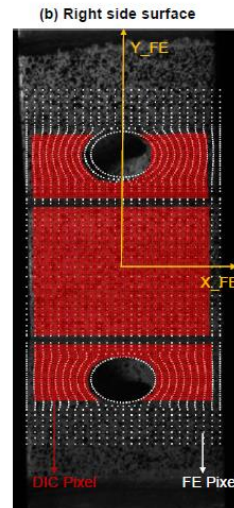
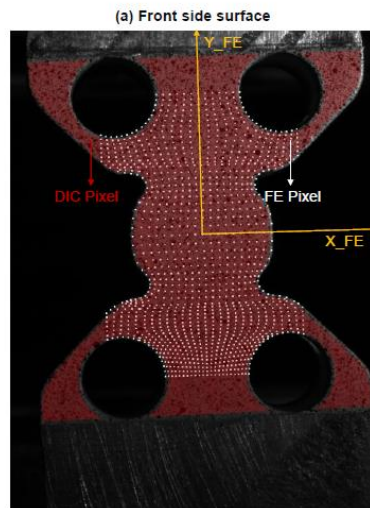
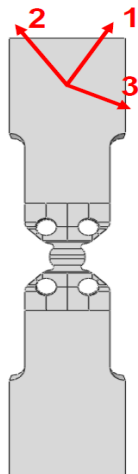
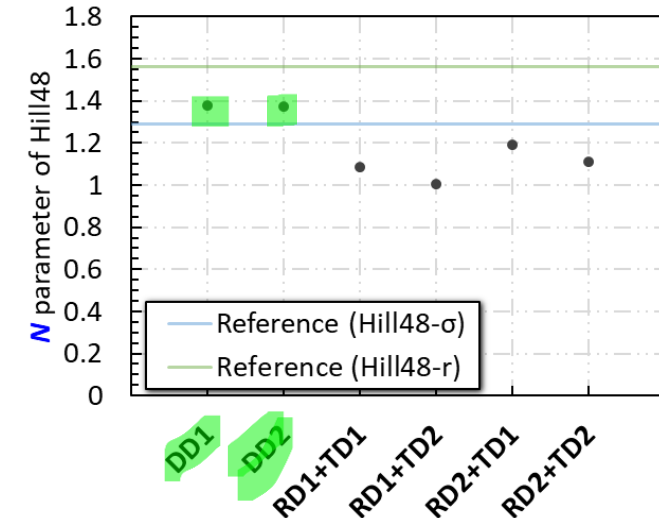
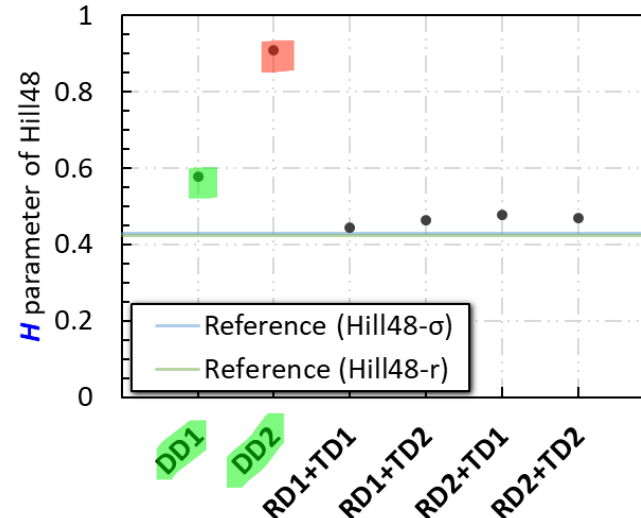
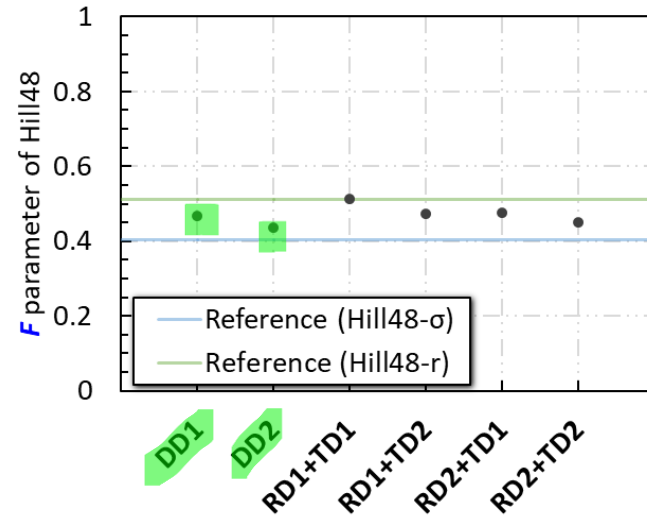
MT2.0



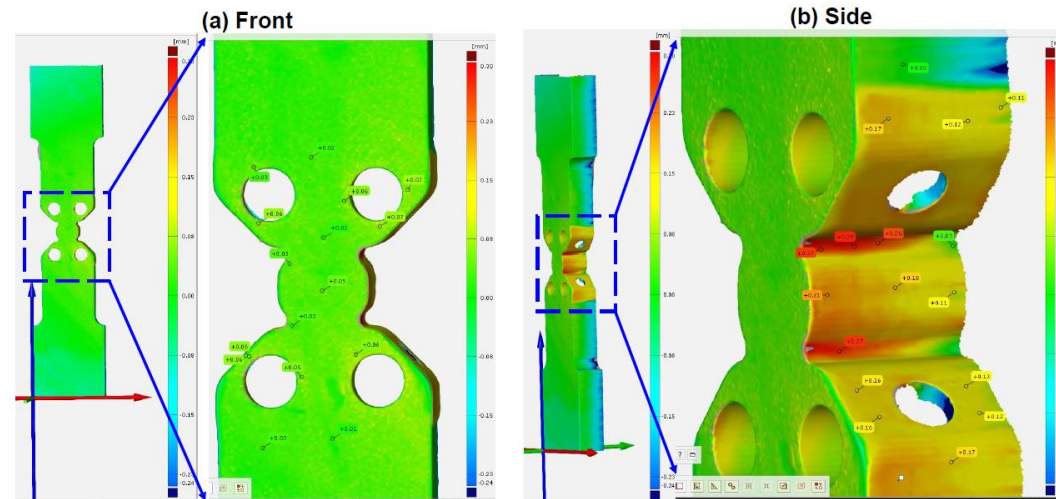
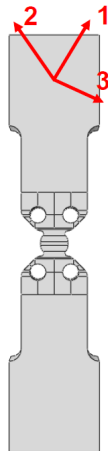
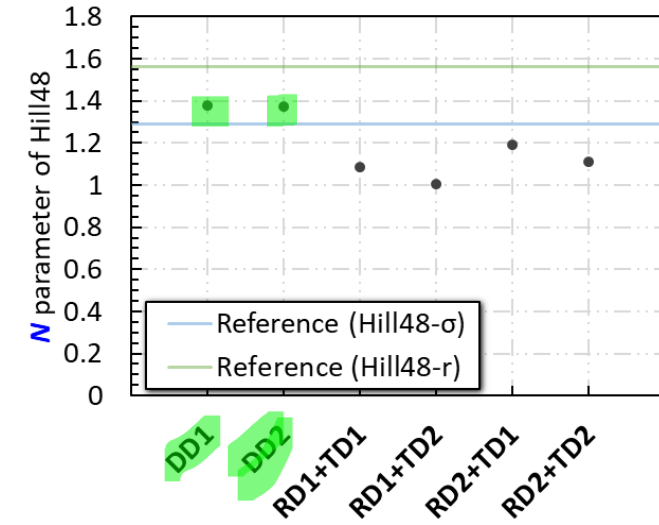
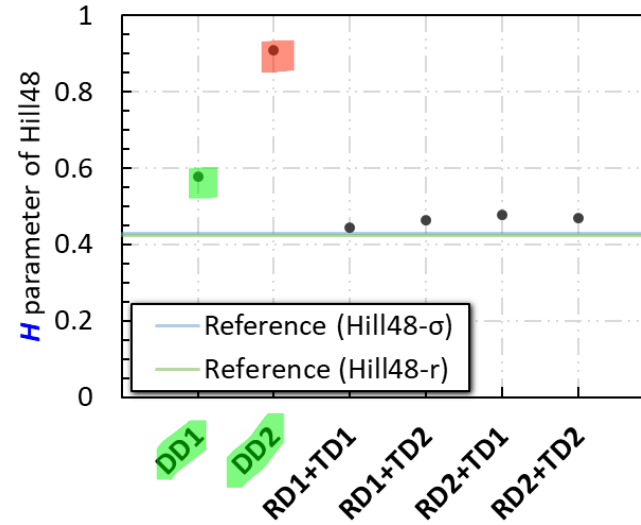
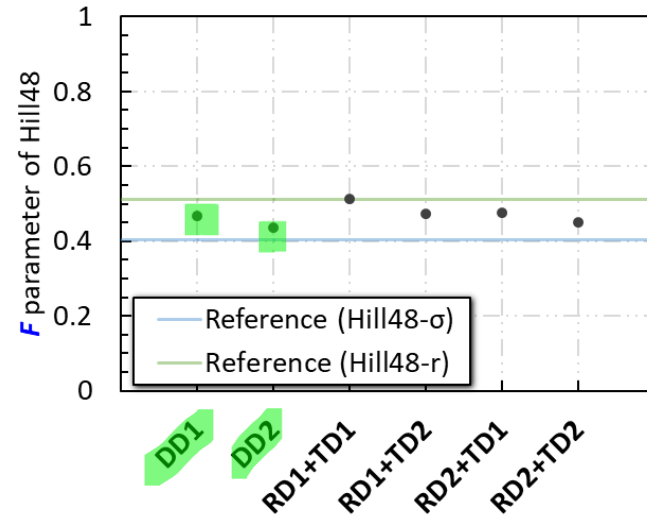
MT2.0: Experimental validation – Robustness



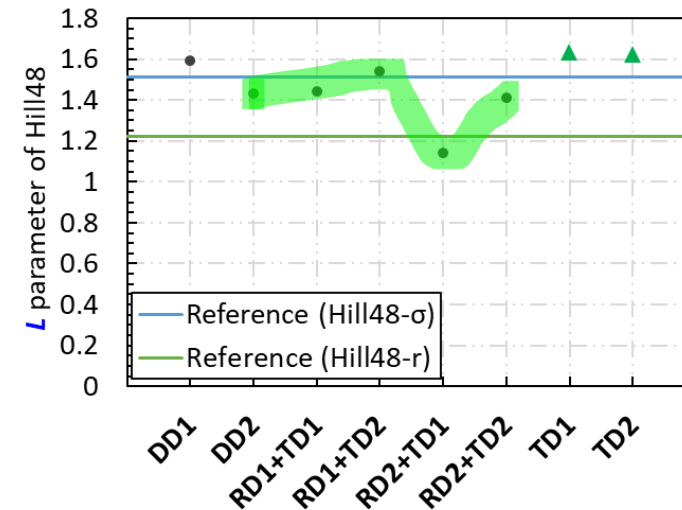
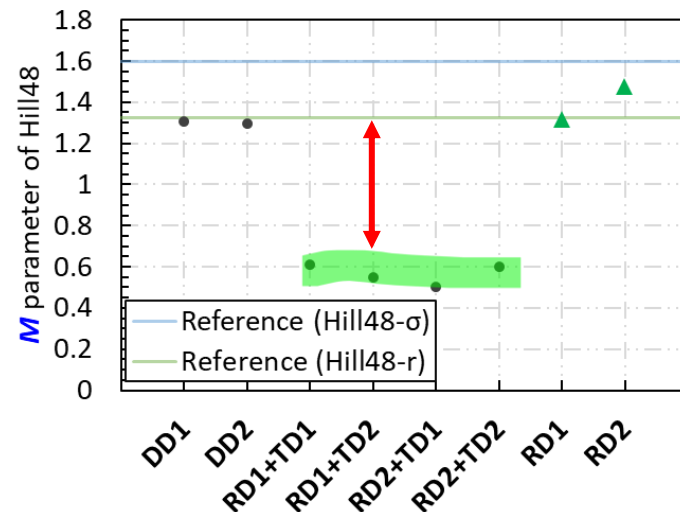
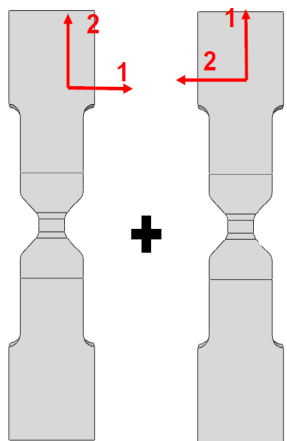
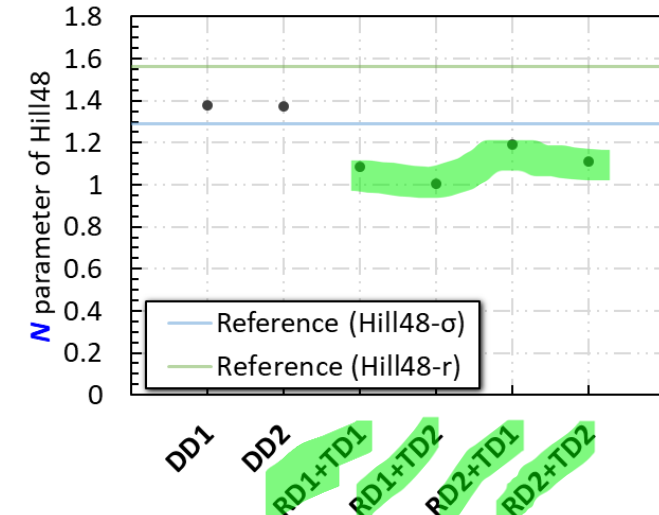
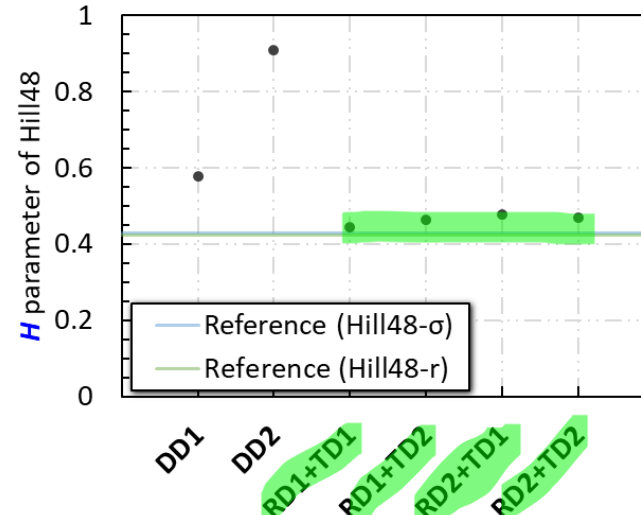
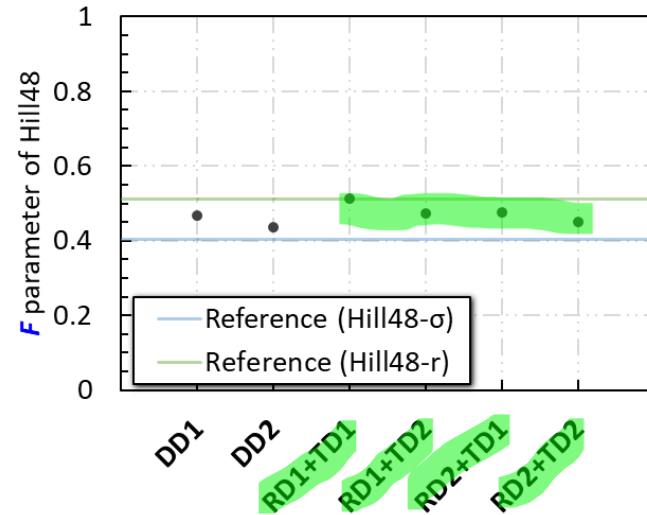
MT2.0: Experimental validation – Robustness



MT2.0: Experimental validation – Robustness



MT2.0: Experimental validation – Material model error



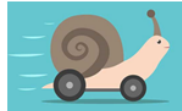
Conclusions MT2.0 for heavy gauge steel

20%



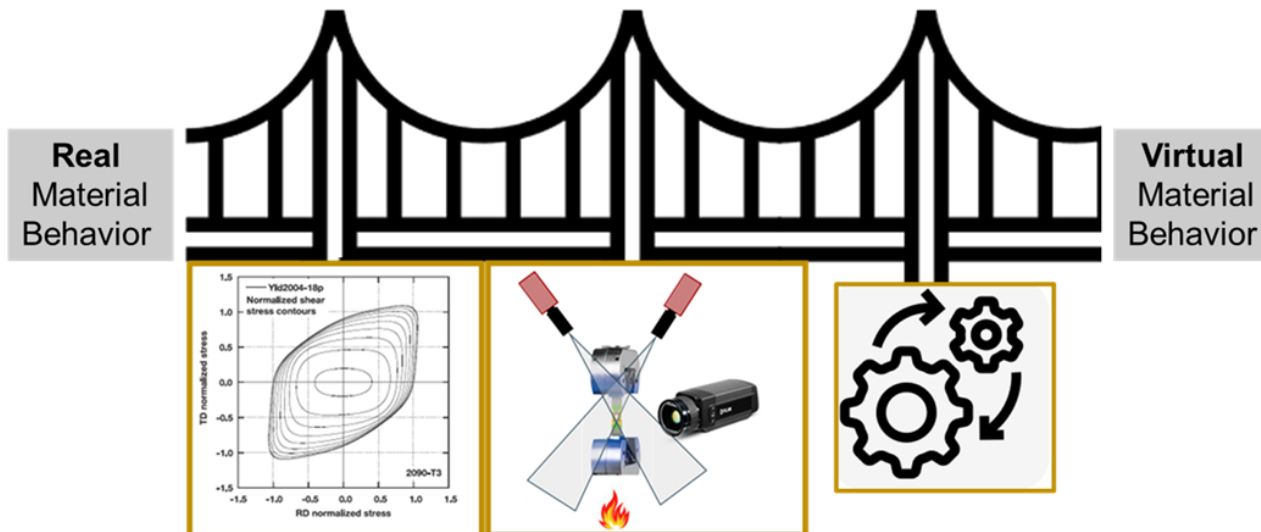
Solid proof of concept

Robust engineering tool

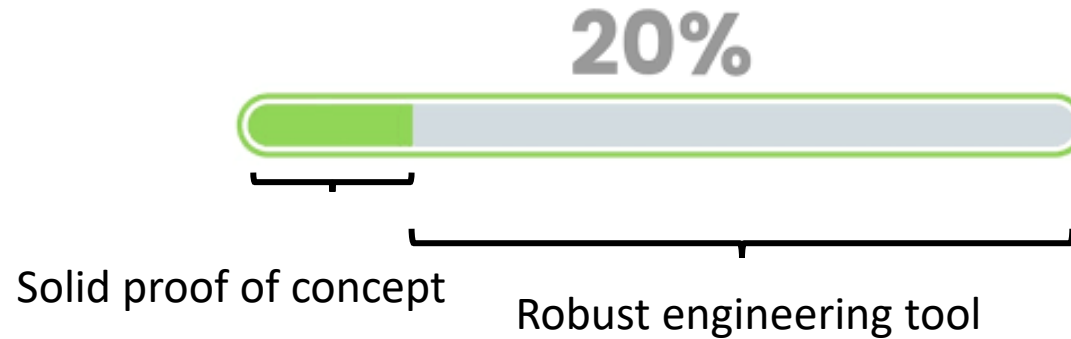


MT2.0

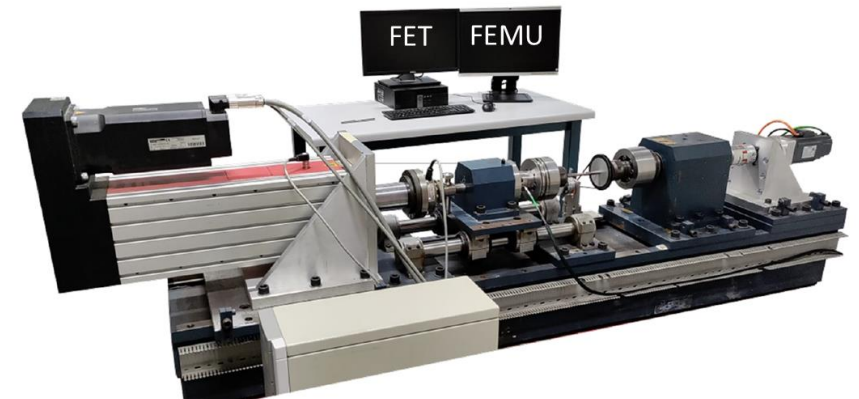
crossing the material twin bridge faster/better



Conclusions MT2.0 for heavy gauge steel



- Simplicity of the specimen is key¹: rather two simple specimens than one very complex.
- An automated design strategy² is still lacking for thick heavy gauge steel.
- Material model selection³ is an open question, there are options⁴ but therefore FEMU methods need to be accelerated.
- DVT is crucial tool (extension to IRT is under way⁵).
- Integrated MT2.0 solutions are required to gain industrial relevance⁶.



¹ PhD Yi Zhang

⁴ PhD Amar Peshave

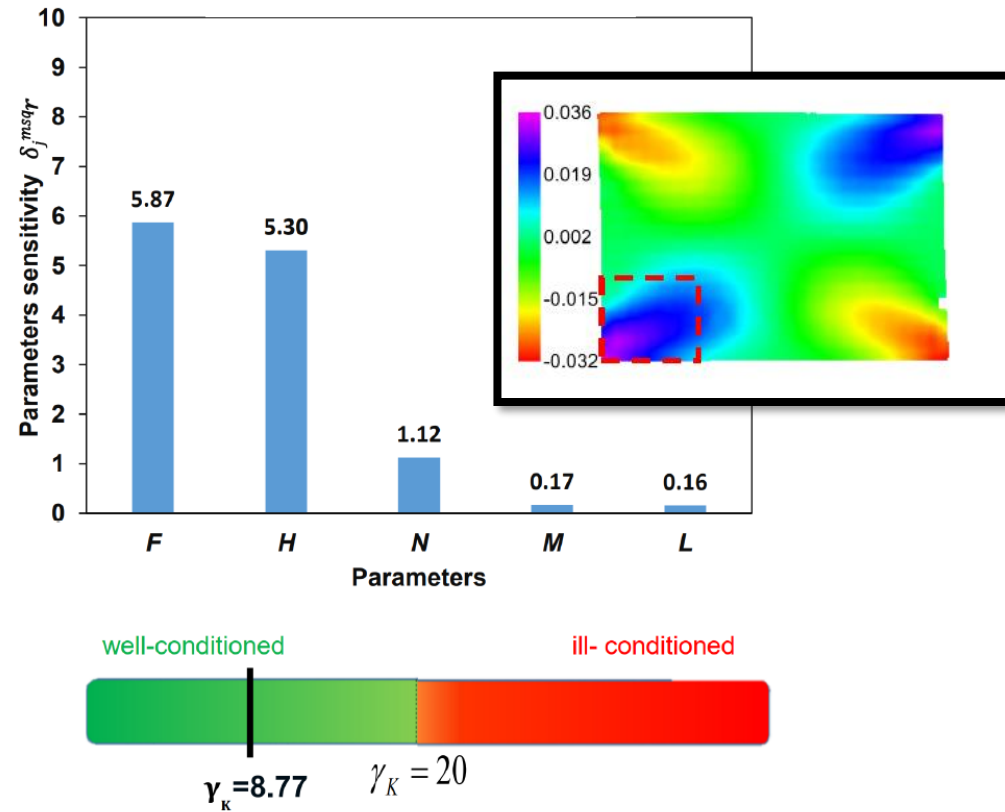
² PhD Mafalda Gonçalves

⁵ PhD Alessandro Lambrughì

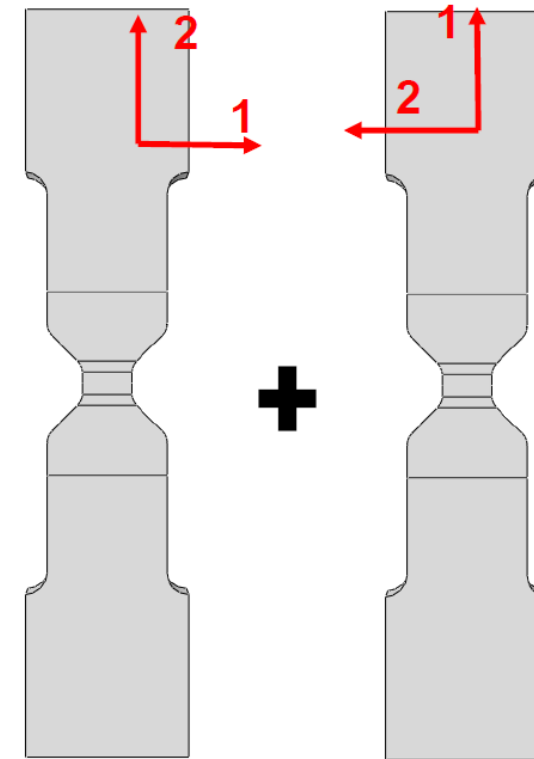
³ PhD Mariana Conde

- Thank you !

Identifiability analysis: maximizing parameter identifiability



Identifiability analysis



Two-specimen approach